

# PUBLIC ROADS

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PUBLIC ROADS ADMINISTRATION

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Photo by Public Buildings Administration

AERIAL VIEW OF WASHINGTON NATIONAL AIRPORT

# PUBLIC ROADS

►►► *A Journal of  
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D. M. BEACH, *Editor*

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*The reports of research published in this magazine are necessarily qualified by the conditions of the tests from which the data are obtained. Whenever it is deemed possible to do so, generalizations are drawn from the results of the tests; and, unless this is done, the conclusions formulated must be considered as specifically pertinent only to described conditions.*

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# STABILIZATION OF GRAVEL RUNWAYS ON WASHINGTON NATIONAL AIRPORT

BY THE DIVISION OF TESTS, PUBLIC ROADS ADMINISTRATION

Reported by HENRY AARON, Associate Highway Engineer and J. A. KELLEY, JR., Assistant Highway Engineer

**T**H E L A N D I N G F I E L D of the Washington National Airport occupies over 500 of the 720 acres comprising the airport. About 325 acres of the landing area is located in what was originally shoal water and mud flats along the Virginia shore of the Potomac River. This low area was filled to an elevation of 12 to 16 feet above the normal water level with material pumped from the river by means of hydraulic dredges. The remainder of the landing field was brought to grade with dry fill obtained during the grading of the adjacent upland areas.

Preliminary borings disclosed that there was a layer of soft mud varying from 5 to 20 feet in thickness over most of the site. Underlying the mud was a stratified deposit of sand, gravel, cobbles, and silt.<sup>1</sup> In order to obtain as stable a foundation as possible for the runways and to reduce the differential and ultimate settlements likely to occur, the runway areas were trenched to a width of 200 feet and a depth of 12 feet below mean low water or to hard bottom if encountered at less depth.

The excavated trenches were then backfilled with material pumped from borrow pits located in the river on the outskirts of the field.

The material in the borrow pits contained 60 percent of sand and gravel and 40 percent of silt and muck. By placing the pipe lines of the hydraulic dredges longitudinally along the runways, the granular material was collected in the runway areas and the silt and muck floated off to be deposited by ponding in the intermediate areas between and outside of the runways.

The gravel fill was built up to a height of 6 to 8 feet above the final grade of the runways, the additional material serving as a surcharge to hasten consolidation of the newly placed fill material and any compressible material in the foundation below. It served also to furnish gravel for widening the runways and for use in other areas of the airport.

The hydraulic filling was started in December 1938 and completed in December 1939.

The Washington National Airport was built under the joint supervision of several Federal agencies. This report covers the participation of the Public Roads Administration in the stabilization of the gravel runways.

The runways, varying in length from 4,200 to 6,875 feet and surfaced with 3½ inches of bituminous concrete on a stabilized gravel base 9 inches thick, are located almost entirely on what was originally shoal water and mud flats along the Virginia shore of the Potomac River. This low area was filled to an elevation of 12 to 16 feet above the normal water level with material consisting of sand, gravel cobbles, silt, and muck pumped by means of hydraulic dredges from borrow pits located in the river on the outskirts of the field. By placing the pipelines of the hydraulic dredges longitudinally along the runways, the granular material was collected in the runway areas and the silt and muck floated off to be deposited by ponding in the intermediate areas between and outside of the runways.

The gravel in the runways was combined with soil from adjacent upland areas to produce a dense, well-graded, stable base course for the bituminous concrete surfacing. The work of stabilization consisted of scarifying the graded gravel runways, removing oversize stone, adding the proper amount of soil, mixing the gravel and soil by means of cultivators, disk harrows, and plows, compacting with rollers, and shaping with motor graders and drags. The desired gradations, physical properties, and densities were obtained by coordinating the construction operations with laboratory tests performed on the materials and the mixtures.

## STABILIZATION REQUIRED TO PROVIDE UNIFORM SUPPORT FOR PAVEMENT

In October 1939, the Public Roads Administration was requested by the engineering authorities at the Washington National Airport to make a study of the character and quality of the gravel deposited in the runway areas, and to determine what measures should be taken to produce a satisfactory base course for an asphaltic concrete wearing surface. In addition to the four runways, the paving program included taxiways, aprons, access and service roads, parking areas, and the relocation of about 1.75 miles of the Mount Vernon Memorial Highway. The layout of these facilities is shown in figure 1.

The investigation disclosed that the material in the runways did not consist of uniform mixtures of sand and gravel. Instead, the fill contained stratifications and pockets of sand, gravel, and cobbles, and in certain locations layers and pockets of clay and muck were encountered.

The behaviour of the existing runway material under the action of construction traffic showed a large variation in stability. Some portions became well compacted while other sections remained loose and became rutted. Sponginess and rutting were observed in the mucky areas. These conditions indicated the need for stabilization in order to provide satisfactory support over the entire area to be paved.

The design called for a stabilized base 9 inches thick after compaction for the runways and taxiways located in the hydraulic fill area and a 12-inch base constructed in two 6-inch courses for the dry fill areas of the landing field as well as for the relocated Mount Vernon Memorial Highway over Four Mile Run. Access roads, service roads, parking zones, and most of the taxiways were designed to have a 5-inch compacted gravel lower course and an 8-inch stabilized gravel upper course. The stabilized base extended 3 feet beyond the edges of the asphaltic concrete surface which was 200 feet wide on the North-South and the Northwest-Southeast runways, 150 feet on the Northeast-Southwest and East-West runways, and 75 feet on the taxiways. Typical cross sections are shown in figure 2.

<sup>1</sup> Washington National Airport, by Lt. R. C. Tripp, Corps of Engineers, U. S. Army. The Military Engineer, September-October 1939.

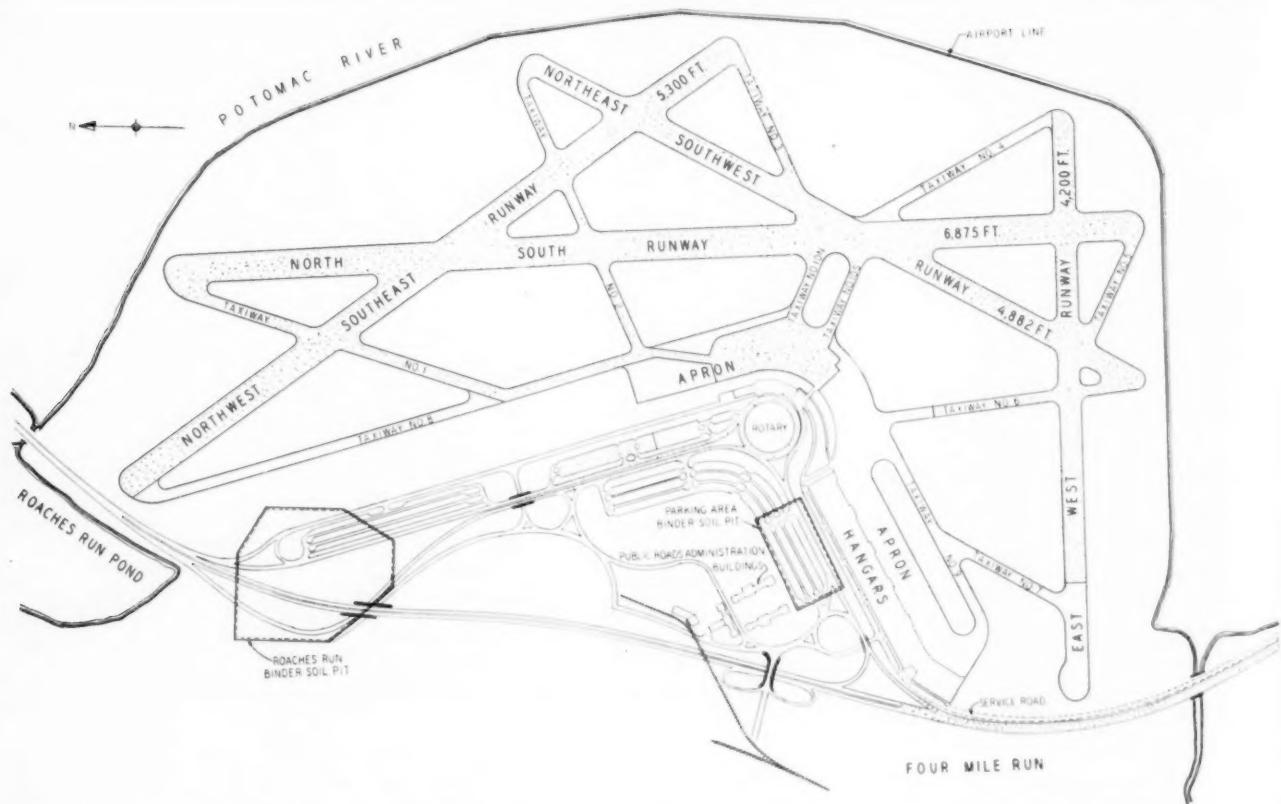
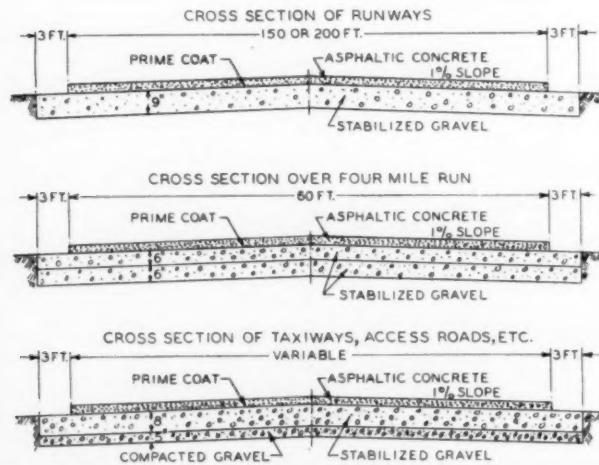


FIGURE 1.—LAYOUT OF RUNWAYS, TAXIWAYS, APRONS, AND ROADS AT THE WASHINGTON NATIONAL AIRPORT. SHADED AREAS INDICATE WORK COMPLETED DURING 1940.



**FIGURE 2.—TYPICAL PAVING CROSS SECTIONS, WASHINGTON NATIONAL AIRPORT.**

Construction of the stabilized base was commenced on March 6, 1940, and continued until the end of the year when the stabilization operations were suspended for the winter. The work completed during this construction period, amounting to approximately 544,000 square yards of stabilized base and indicated by the shaded areas on figure 1, may be summarized as follows:

Facility:	Area completed, square yards
Runways	392,600
Taxiways	87,900
Apron	31,000
Mount Vernon Memorial Highway	21,000

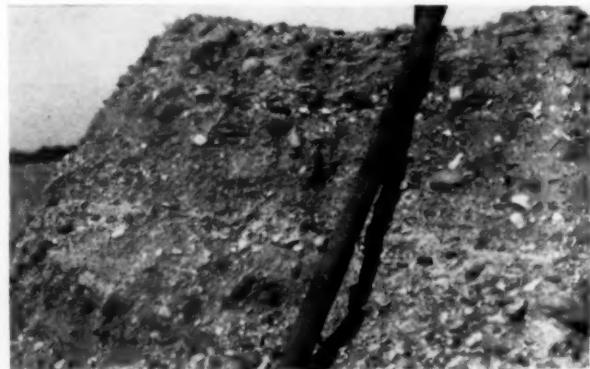


FIGURE 3.—TYPICAL FORMATION OF GRAVEL DEPOSITED BY PUMPING OPERATIONS.

#### **Facility—Continued.**

### **Access roads.**

#### **Parking zones.**

*Area completed,  
square yards*

This report, covering the participation of the Public Roads Administration in the base course stabilization, describes the character of the materials, the methods of construction and control, the sampling, testing, and proportioning of materials, and presents a summary of the results obtained.

The character of the gravel formations as deposited by the pumping operations is illustrated in figure 3. Tests performed on samples taken from the upper 12 inches of the runways (see table 1) indicated that the material, in general, was a nonplastic mixture of sand and gravel with variable amounts of large rock and

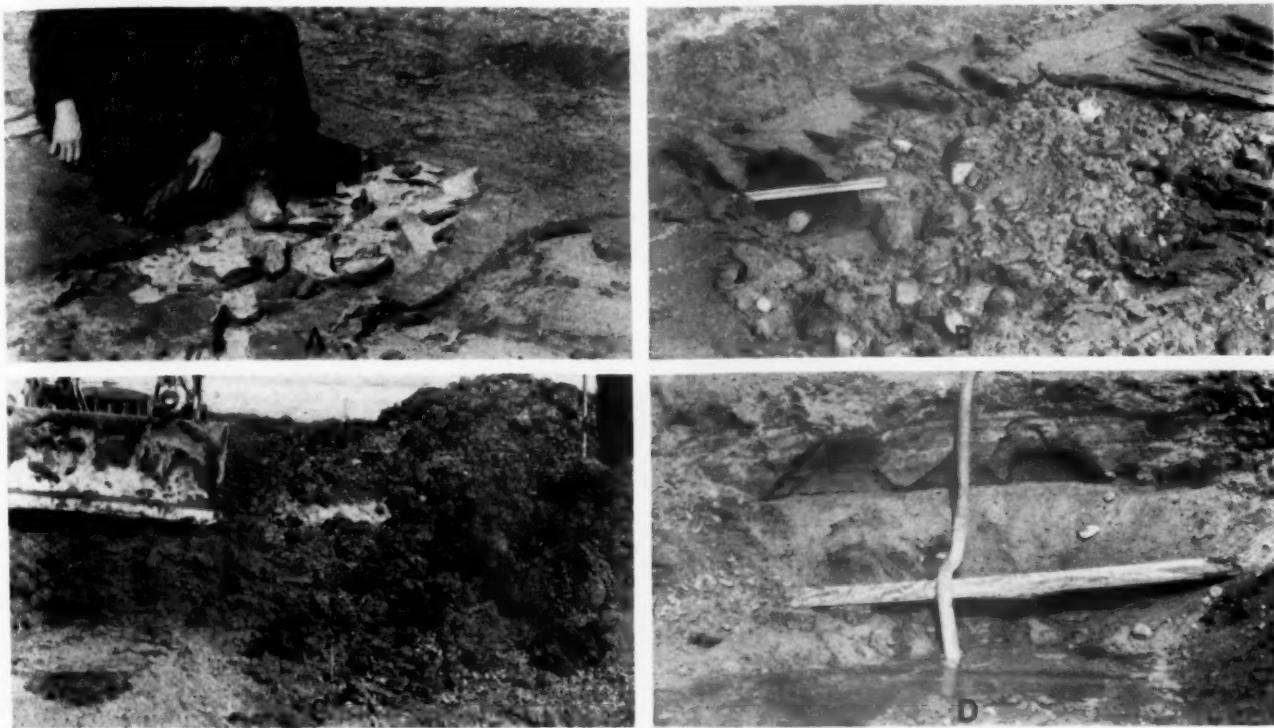


FIGURE 4.—TYPICAL EXAMPLES OF POCKETS AND LAYERS OF MUCK AND SAND. A, THIN LAYERS OF MUCK; B, POCKET OF MUCK, GRAVEL, AND ENTRAPPED WATER; C, DEEP POCKET OF SOFT MUCK; AND D, SANDY DEPOSIT WITH THIN LAYERS OF MUCK.

cobbles. The percentage of large rock varied considerably from place to place. After removing this material, however, the remaining sand and gravel was fairly well graded but was lacking in material passing the No. 200 sieve. As a result, it was decided to stabilize the gravel by the addition of a binder soil from the adjacent upland area.

In addition to variations in the amount of large rock in the gravel fill, layers and pockets of muck and fine sand were encountered in many locations. These conditions are illustrated in figure 4. Mechanical analyses and physical properties typical of these materials are given in table 2.

TABLE 1.—Results of tests performed on samples typical of gravel pumped into runways of Washington National Airport

SIEVE ANALYSIS

	Sample No.—							
	1	2	5	7	9	12	13	16
<b>Percentage passing:</b>								
2-inch sieve	86	100	100	92	96	63	75	100
1½-inch sieve	86	95	96	89	93	58	70	98
1-inch sieve	85	85	95	81	89	53	62	93
¾-inch sieve	80	71	92	71	82	46	56	86
½-inch sieve	65	53	79	51	62	36	45	71
No. 4 sieve	53	40	66	37	44	29	36	58
No. 10 sieve	42	34	55	25	32	24	29	48
No. 40 sieve	25	27	36	34	13	11	18	34
No. 200 sieve	3	2	5	7	2	2	5	5

PHYSICAL CONSTANTS OF MATERIAL PASSING NO. 40 SIEVE

Liquid limit	(1)	(1)	(1)	230	(1)	(1)	(1)
Plasticity index				9			

<sup>1</sup> Nonplastic.

<sup>2</sup> Sample No. 7 was taken in an area containing a thin layer of muck.

TABLE 2.—Typical analyses of muck and sandy material

	Sand	Muck
Mechanical analysis:		
Coarse sand (2.0 to 0.25 mm.)	percent	16
Fine sand (0.25 to 0.05 mm.)	do	61
Silt (0.05 to 0.005 mm.)	do	16
Clay (smaller than 0.005 mm.)	do	57
Physical properties:		
Liquid limit	19	71
Plasticity index	(1)	27
Shrinkage limit		31
Shrinkage ratio		1.4
Centrifuge moisture equivalent	7	51
Field moisture equivalent	31	53

<sup>1</sup> Nonplastic.

The formations consisting largely of fine sand were quite spongy when associated with a high water table resulting from blocked drainage. These areas were drained but the material itself was too fine to produce a stabilized base by means of an admixture of binder soil. It was necessary to add both gravel and binder soil.

The muck had physical characteristics typical of the group A-8 subgrades. It was extremely unstable and had to be removed and replaced with gravel during the construction of the stabilized base.

FOUR DIFFERENT GRADINGS PERMITTED IN STABILIZED MIXTURES

Two portions of the upland area, one at Roaches Run and the other at the proposed parking zone south of the Public Roads Administration laboratories (fig. 1), were designated as the locations most convenient for obtaining binder soil without interfering with the grading operations. Accordingly, a soil survey of these areas was made to determine the character and quantities of soils available for use as binder material for stabilization.

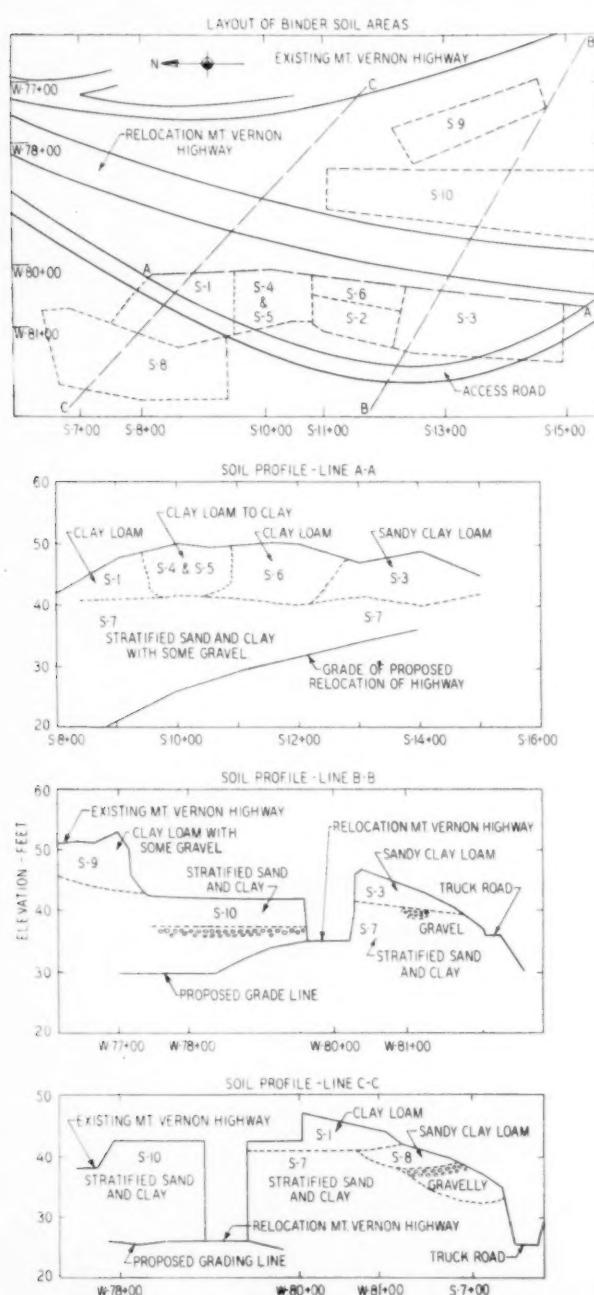


FIGURE 5.—LAYOUT AND SOIL PROFILES OF BINDER SOIL PIT AT ROACHES RUN.

Borings were made to determine the soil profiles and samples representative of the different layers of the profile were taken and tested in the Public Roads Administration soils laboratory. The soil profiles for the Roaches Run pit are shown on figure 5 and the results of tests performed on the samples of soil are given in table 3. The soil profiles and test results for the parking area pit are presented in figure 6 and table 4.

With the exception of the material designated S-7, all of the soils encountered in the two pits were found to be satisfactory for use as binder soil. The S-7 material was too sandy for this purpose. Approximately 24,000 cubic yards of binder soil of acceptable quality was available in the Roaches Run pit and about 27,000 cubic yards in the parking area pit, making a total of

TABLE 3.—Results of tests performed on samples from Roaches Run binder soil pit, Washington National Airport

SIEVE ANALYSIS

	Sample No.—									
	S-1	S-2	S-3	S-4	S-5	S-6	S-7	S-8	S-9	S-10
Percentage passing:										
No. 10 sieve	100	100	100	100	100	100	100	100	100	100
No. 40 sieve	98	96	98	99	99	99	95	96	99	97
No. 60 sieve	94	74	89	97	95	95	75	85	95	83
No. 200 sieve	66	32	48	82	70	65	25	49	66	40

HYDROMETER ANALYSIS OF MATERIAL PASSING NO. 10 SIEVE

Sand, percent	41	72	57	24	37	42	79	57	43	65
Silt, percent	31	10	20	42	30	31	10	20	36	29
Clay, percent	28	18	23	34	33	27	11	23	21	15

PHYSICAL CONSTANTS OF MATERIAL PASSING NO. 40 SIEVE

Liquid limit	26	23	27	33	31	29	19	23	25	19
Plasticity index	9	4	9	11	12	9	0	6	7	2

TABLE 4.—Results of tests performed on samples from parking area binder soil pit, Washington National Airport

SIEVE ANALYSIS

	Sample No.—					
	P-1	P-2	P-3	P-4	P-5	P-6
Percentage passing:						
No. 10 sieve	100	100	100	100	100	100
No. 40 sieve	99	99	99	99	99	99
No. 60 sieve	97	87	97	94	98	90
No. 200 sieve	76	40	78	63	83	57

HYDROMETER ANALYSIS OF MATERIAL PASSING NO. 10 SIEVE

Sand, percent	31	65	28	43	22	48
Silt, percent	37	17	38	30	36	28
Clay, percent	32	18	34	27	42	24

PHYSICAL CONSTANTS OF MATERIAL PASSING NO. 40 SIEVE

Liquid limit	30	22	31	28	38	25
Plasticity index	10	4	10	10	17	8

51,000 cubic yards which was more than sufficient for the proposed stabilization.

The acceptable soil materials in general were yellowish and yellowish-red sandy loams and clay loams. They were friable in consistency and could be readily pulverized. With respect to the gradations of the samples, the fraction passing the No. 200 sieve ranged from 32 to 83 percent. The liquid limits varied from 19 to 38 and the plasticity indexes from 2 to 17.

In order to provide for variations in the materials encountered in the runways, four different gradings were permitted in the stabilized mixtures. They were based on the maximum size of the gravel in the mixture after the large rock and cobbles had been removed. The permissible gradings limits are given in table 5.

It was required that the gravel be combined with binder soil in such proportions that the resulting mixture would fall within the limits of grading B, C, D, or E, whichever best fitted the material available. However, since it was desired to use any suitable material existing in the runways that would be satisfactorily stabilized, some tolerance from the limits given in table 5 was allowed at the discretion of the engineer.

In addition to the grading requirements, it was required that the fraction passing the No. 200 sieve

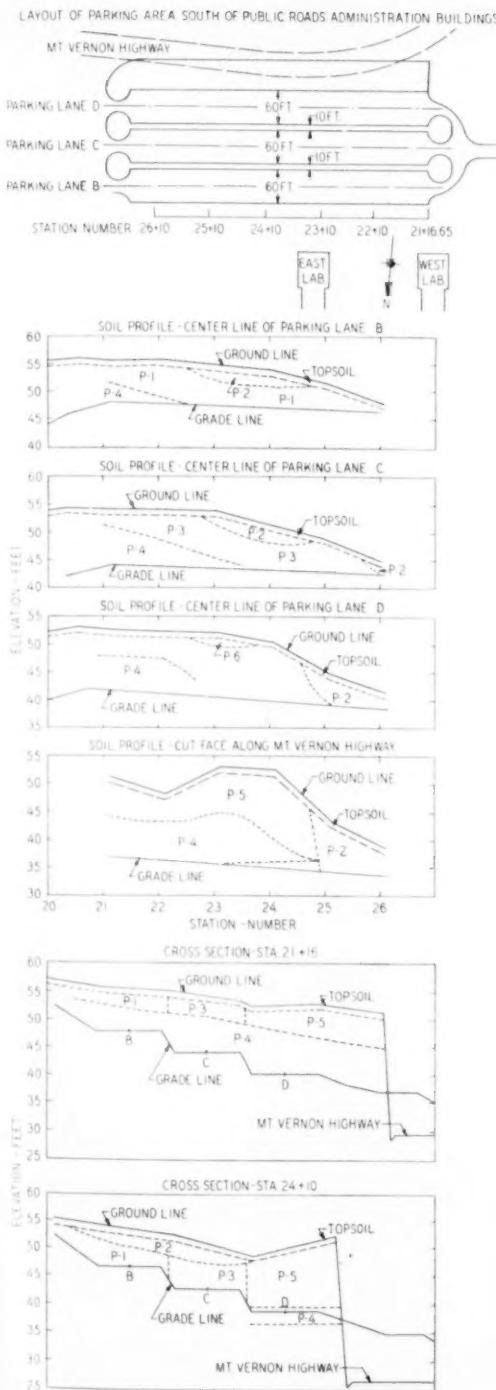


FIGURE 6.—LAYOUT, SOIL PROFILES, AND CROSS SECTIONS OF BINDER SOIL PIT AT PARKING AREA.

should be less than one-half the fraction passing the No. 40 sieve, and also that the fraction passing the No. 40 sieve should have a liquid limit not greater than 25 and a plasticity index not greater than 6.

Control over the base stabilization in accordance with these requirements was accomplished by coordinating the construction operations with the tests performed on the raw materials and the mixtures. This work was directed from a portable field laboratory (fig. 7) located on the runways.



FIGURE 7.—PORTABLE LABORATORY (CENTER) AND OFFICES ON RUNWAYS.

TABLE 5.—Gradation requirements for stabilized mixtures

Sieve designation	Percentage by weight passing square mesh sieves			
	Grading B	Grading C	Grading D	Grading E
3-inch	100			
2-inch	65-100	100		
1½-inch		70-100		
1-inch	45-75	55-85	100	
¾-inch	50-80	70-100		90-100
No. 4	30-60	40-70	50-80	70-100
No. 10	25-50	30-60	35-65	50-90
No. 40	20-40	20-50	25-50	35-80
No. 200	10-25	10-30	15-30	20-50
	3-10	5-15	5-15	8-25

The rough grading was generally performed by bulldozers which pushed the surcharged fill material off to the sides of the area to be stabilized. When gravel was needed in other locations, it was pushed into large piles by the bulldozers and loaded into trucks by means of a dragline (fig. 8-A). Motor patrol graders were used to bring the runway to approximate grade and cross section.

Many areas containing unstable mucky materials were encountered during the grading operations. When the muck was in the form of seams or thin layers, it was excavated by means of large tractor-drawn scrapers (fig. 8-B). Deep pockets were removed with draglines (fig. 8-C). All muck deposits were removed to a minimum depth of 3 feet below subgrade elevation and replaced with gravel.

After the grading was completed, the runway material was scarified with a heavy-duty rooter (fig. 8-D) to an approximate depth of 12 inches. The scarified gravel was then further loosened with a field cultivator and all oversized stone brought to the surface (figs. 8-E and 8-F) were removed by hand. These operations were continued until the depth to be stabilized was, for all practical purposes, free of all stones larger than about 3 inches and other objectionable material such as clay balls.

When sections of the runway had been satisfactorily cleared of oversize stone and other undesirable material, samples were taken from the 12 inches of loosened material and their gradations were determined in the laboratory. At the same time, samples of binder soil were obtained from the pit and analyzed. The percentage of binder soil to be added to the gravel and the area to be covered by each load of binder soil was calculated from the results of these tests.

#### MATERIALS THOROUGHLY MIXED AND COMPACTED

As the removal of the stone from a section sufficiently large to permit satisfactory operation of the mixing equipment was nearing completion, a crew of

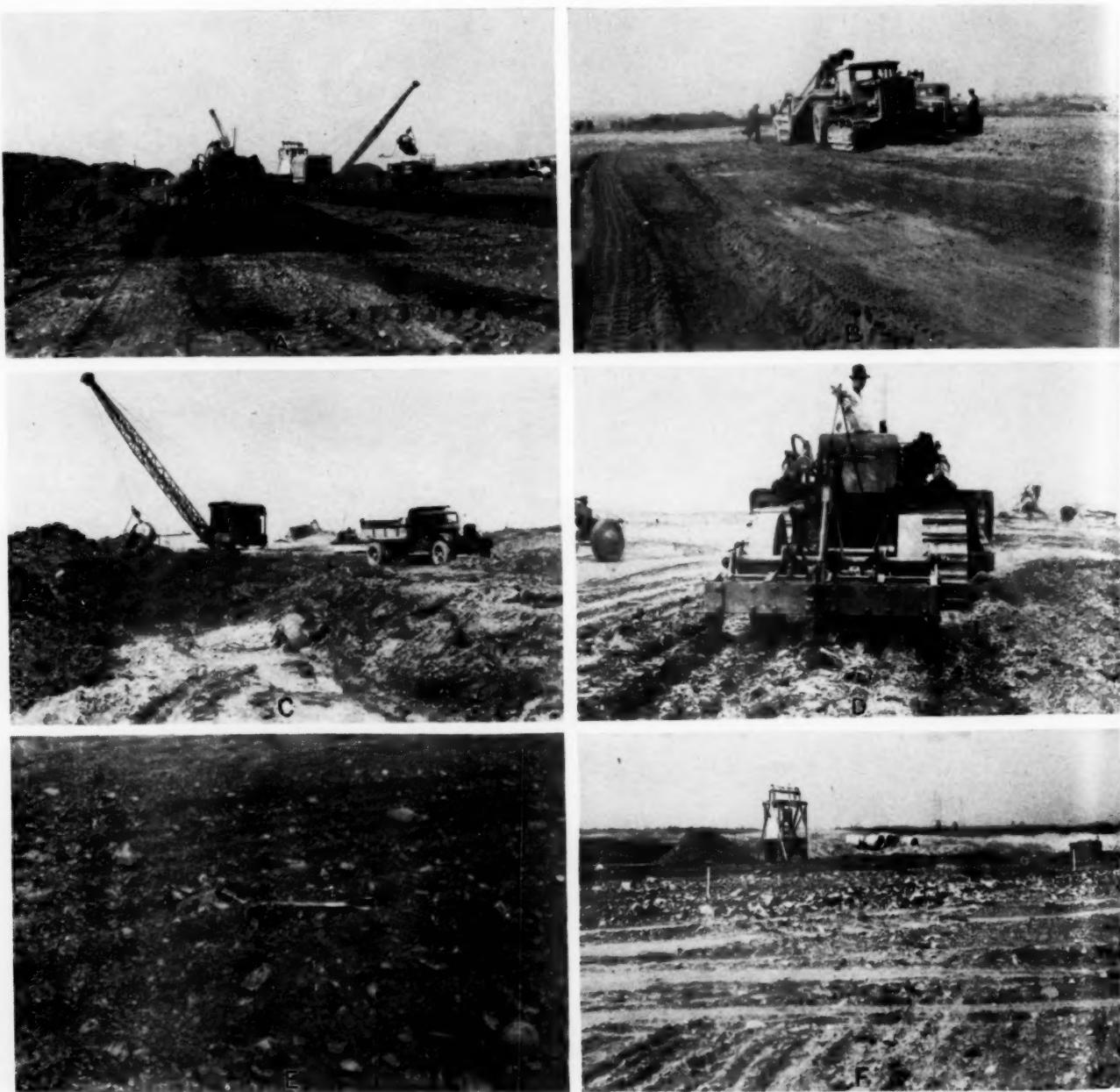


FIGURE 8.—CONSTRUCTION OF RUNWAYS: A, GRADING OPERATIONS; B, THIN LAYERS OF MUCK BEING EXCAVATED BY SCRAPER; C, DEEP MUCK BED BEING EXCAVATED BY DRAGLINE; D, SCARIFYING MATERIAL WITH HEAVY-DUTY ROOTER; E, OVERRSIZE STONE BROUGHT TO SURFACE BY SCARIFYING; AND F, OVERRSIZE STONE IN EXCESSIVE AMOUNTS GENERALLY ENCOUNTERED AT RUNWAY INTERSECTIONS.

laborers was sent to the binder soil pit where a bulldozer had stripped off the topsoil containing vegetable matter and had pushed up a large pile of approved binder soil. The binder soil was loaded by hand into transportable, bottom dump, 2-cubic yard boxes (fig. 9-A), hauled to the runways, dumped (fig. 9-B), and spread by hand over an area previously staked out in accordance with instructions issued by the testing laboratory.

The first step in the mixing was to cut in the binder soil by means of the field cultivator (fig. 9-C). This was followed by one trip with a two-way tandem disk harrow (fig. 9-D) equipped with disks 28 inches in diameter. In order to facilitate the distribution of the

binder soil through the full depth to be stabilized, the disked material was turned with a four-bottom gang plow (fig. 9-E). Mixing with the disk harrow and cultivator was then continued until the binder soil and gravel were thoroughly and uniformly mixed to the specified depth.

Water was applied (fig. 9-F) whenever necessary during the mixing operations. The need for water was determined by the requirements for compaction. Tests made on the base course material in locations where satisfactory compaction was obtained showed that 5 to 7 percent of moisture was required to give the desired results. This checked very closely with the optimum moisture content of 10 percent (American



FIGURE 9.—STABILIZATION OF RUNWAYS: A, LOADING BINDER SOIL IN 2-CUBIC YARD BOXES; B, DEPOSITING AND SPREADING BINDER SOIL; C, CUTTING IN BINDER SOIL WITH FIELD CULTIVATOR; D, MIXING WITH TWO-WAY TANDEM DISK HARROW; E, TURNING DISKED MATERIAL WITH FOUR-BOTTOM GANG PLOW; AND F, SPRINKLING DURING MIXING OPERATIONS.

Association of State Highway Officials' Method T 99-38) on the material passing the No. 4 sieve, which averaged about 60 percent of the total mixture.

While the mixing was in progress, frequent checks were made on the moisture content, the uniformity of the mixture, and the depth of the mixed material.

The loose mixture of gravel and soil was bladed to approximate cross section with a motor patrol and then compacted with multi-wheel, pneumatic-tired rollers (fig. 10-A) weighing about 6 tons. This rolling was continued until an unyielding surface was produced under the weight of these rollers. At least two trips were required to obtain this condition. The appearance of the compacted mixture is illustrated in figure 10-B. Final compaction was obtained by means of a three-wheel, 10-ton roller (fig. 11-A). The motor patrol

(fig. 11-B) and a multiple-blade drag (fig. 11-C) were used to keep the surface properly shaped during rolling.

The surface was maintained in a moist condition by sprinkling while these operations were in progress.

Weak spots which developed in the base or subgrade during the rolling were examined by means of test pits and corrected according to the needs of the particular case. A further check on the subgrade stability was obtained by operating a 12-ton, solid-tired truck (fig. 12-A) over the compacted surface. A failure due to weak subgrade is shown in figure 12-B.

After the base had been compacted to a minimum dry density of 130 pounds per cubic foot, the elevation and cross section was checked by an engineering party. Final shaping consisted of cutting the high spots and filling in low areas in accordance with stakes driven to

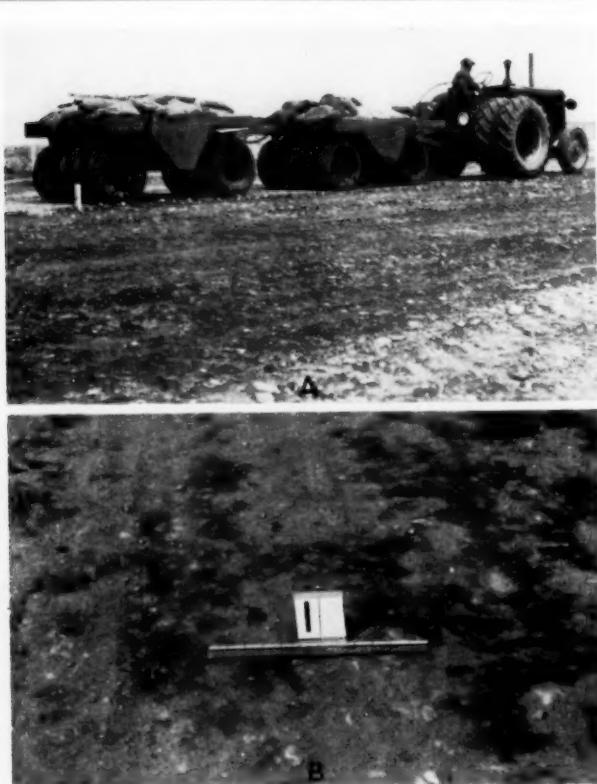


FIGURE 10.—A, COMPACTING STABILIZED BASE WITH PNEUMATIC-TIRED ROLLERS; AND B, APPEARANCE OF BASE AFTER COMPACTING WITH PNEUMATIC-TIRED ROLLERS.

grade elevation at 25-foot intervals. This work was performed by hand or by motor patrol depending on the size of the area to be corrected. The surface was then finished by rolling with an 8-ton tandem roller (fig. 12-C). The appearance of the completed base course is shown in figure 12-D.

The quality of the stabilized mixture was checked by tests performed on samples taken at regular intervals after the mixing was completed. When the results of tests indicated an unsatisfactory mixture at a certain location, additional samples were obtained in sufficient number to determine the limits of the area in this condition. All such areas were reconstructed.

The final step in the stabilization procedure was an application of tar prime at a rate of about 0.25 gallon per square yard. Application of the tar was not permitted until the base course conformed with all the requirements relating to quality of mixture, density, and stability.

The same procedure was followed for each layer of the two-course construction on the Four Mile Run fill and for the upper 8 inches on the taxiways, access roads, etc. (see fig. 2).

#### STABILIZED MIXTURES TESTED TO DETERMINE CONFORMITY WITH REQUIREMENTS

The results of the sieve analyses performed on the samples of stabilized mixtures from the runways are summarized in table 6. These results are shown graphically in figure 13. The samples were grouped into gradation ranges corresponding as closely as possible to the grading requirements given in table 5.

None of the samples had a gradation typical of the B grading. This grading was included in the require-

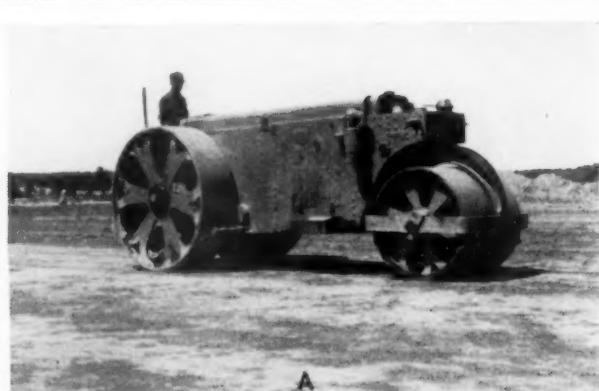


FIGURE 11.—A, COMPACTION WITH 3-WHEEL, 10-TON ROLLER; SHAPING, DURING ROLLING, WITH MOTOR PATROL (B), AND WITH MULTIPLE BLADE DRAG (C).

ments on the basis of materials represented by samples 12 and 13 in table 1. However, practically all of the material remaining after removal of the oversize stone during the construction operations was smaller than 2 inches. Only one sample had more than 10 percent retained on the 2-inch sieve and was included with the samples in grading C.

The range in gradations designated D-E was made necessary by the fact that almost all the gravel samples had some material retained on the 1-inch sieve but many of these could not be placed in the C or D grading because of the high percentages passing the smaller-sized sieves. Many of the samples with material coarser than 1 inch had more than 80 percent smaller than the  $\frac{3}{4}$ -inch sieve. These samples generally had more material passing the No. 10 and No. 40 sieves, even before the addition of binder soil, than was permitted in the specifications for the C and D gradings. Since binder soil was required in practically all instances,

TABLE 6.—Summary of results of sieve analyses performed on stabilized mixtures from runways on Washington National Airport

RANGE IN GRADATION<sup>1</sup>

Sieve designation	Percentage by weight passing square mesh sieves			
	Grading C	Grading D	Grading D-E	Grading E
2-inch	89-100	93-100	100	-----
1½-inch	80-100	86-100	91-100	100
1-inch	72-85	86-92	86-100	95-100
¾-inch	63-80	75-80	81-90	91-100
½-inch	49-65	51-70	63-79	78-91
No. 4	40-56	38-60	47-70	65-83
No. 10	34-47	29-53	37-64	54-76
No. 40	22-35	16-36	19-45	25-57
No. 200	4-13	3-13	4-14	3-19

AVERAGE GRADATION

2-inch	99	100	100	-----
1½-inch	89	96	98	100
1-inch	81	88	92	98
¾-inch	75	78	86	95
½-inch	61	62	71	85
No. 4	51	51	60	74
No. 10	43	42	50	63
No. 40	27	26	30	41
No. 200	8	8	8	11

<sup>1</sup> Range in gradation shows the maximum and minimum percentages passing each sieve for the particular group of samples falling within the grading band indicated.

the gradations of the resulting mixtures could not possibly fall within the limits specified. For this reason, all samples having between 80 and 90 percent passing the ½-inch sieve were included in the D-E grading while those having more than 90 percent finer than the ½-inch sieve were placed in the E grading.

The samples having 80 percent or less passing the ¾-inch sieve were placed in the C grading if the amount smaller than the 1-inch sieve did not exceed 85 percent and in the D grading when the percentage finer than the 1-inch sieve was greater than 85 percent.

The ratios of the fractions passing the No. 200 sieve to the fractions passing the No. 40 sieve ranged from 0.14 to 0.50 with an average of 0.27 for all the samples from the runways.

With respect to the physical properties of the fractions passing the No. 40 sieve, the results of tests may be summarized as follows:

Maximum liquid limit	23
Average liquid limit	18
Maximum plasticity index	6
Average plasticity index	1

A liquid limit of 25 and a plasticity index of 6 were the maximum permitted. In the design of the mixture an attempt was made to hold the plasticity index to 3 or less in order to insure a stable base course under adverse moisture conditions. Only 4 percent of the samples tested had plasticity indexes higher than 3 while 36 percent had plasticity indexes of zero. Another 36 percent were so granular that the plasticity index could not be determined. Of interest in this connection is the fact that the nonplastic mixtures were compacted just as readily as those having a measurable plasticity index.

The base course densities obtained on the runways ranged from 126 to 143 pounds per cubic foot with an average dry density of 134 pounds per cubic foot as compared with the density of 135 pounds per cubic foot used in designing the mixture. The low density of 126 pounds per cubic foot was obtained on the northwest end of the Northwest-Southeast runway. This portion of the runway was constructed before arrangements had been made to control the density or to check the stability of the subgrade.



FIGURE 12—A, CHECKING BASE STABILITY WITH A 12-TON, SOLID-TIRED TRUCK; B, FAILURE DUE TO WEAK SUBGRADE; C, FINAL ROLLING WITH AN 8-TON TANDEM ROLLER, AND D, APPEARANCE OF COMPLETED BASE COURSE.

After the minimum density requirement of 130 pounds per cubic foot was established, lower densities were permitted only when the amount of rolling indicated that no increase in density could be obtained. Such conditions were encountered in a few isolated cases where the mixtures were sandy rather than gravelly in character. These mixtures had densities ranging from 128 to 130 pounds per cubic foot.

In addition to the determination of the density of the 9-inch compacted base course, tests were made at three

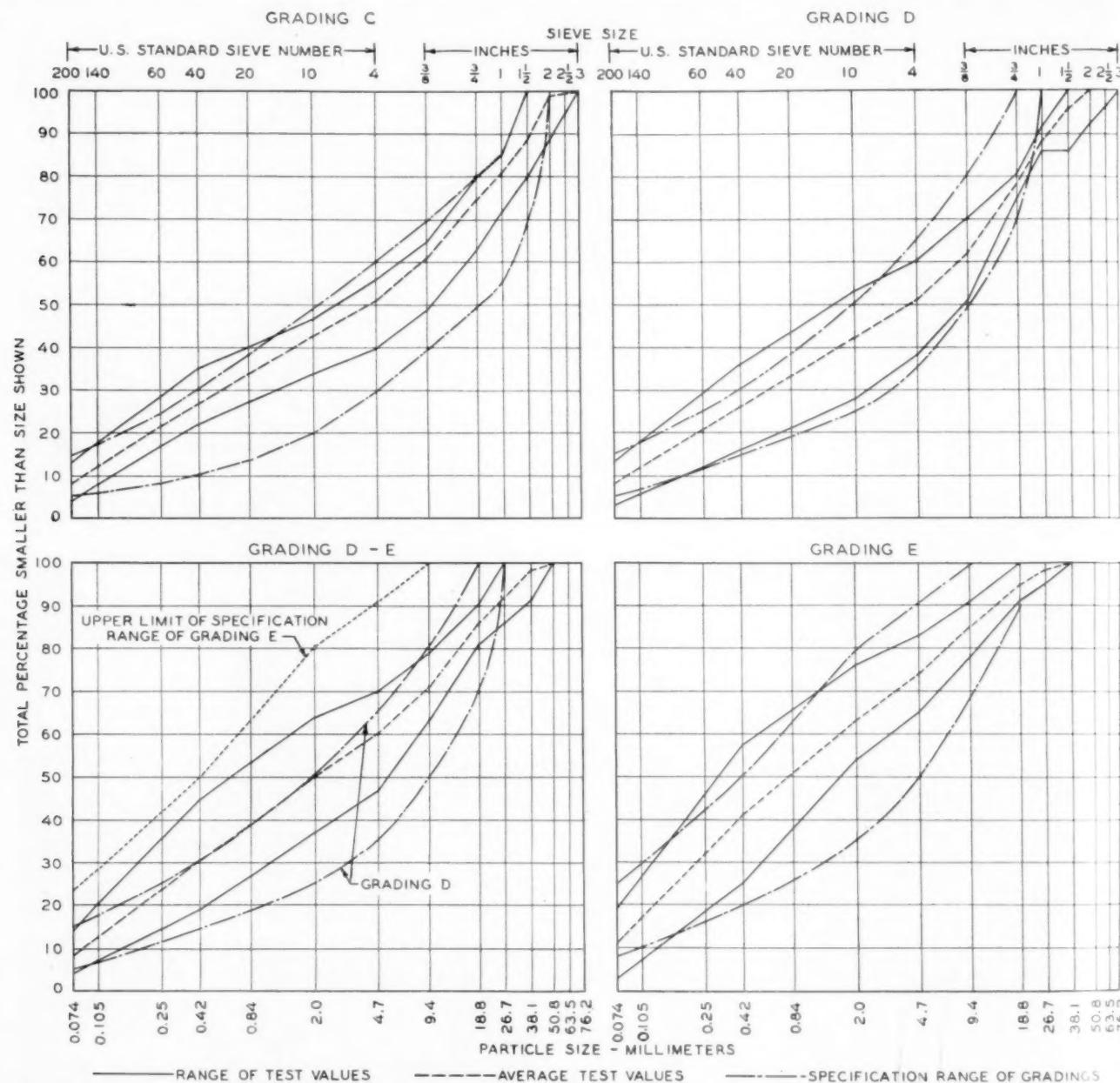


FIGURE 13.—RESULTS OF SIEVE ANALYSES OF STABILIZED BASE COURSE MIXTURES COMPARED WITH SPECIFICATION REQUIREMENTS.

locations on the Northwest-Southeast runway to determine the density of the upper 4½ inches. The two tests at each location were at places not more than 12 inches apart. The results are given in table 7.

TABLE 7.—*Densities of samples from Northwest-Southeast runway*

Station	Thickness tested	Dry density
	Inches	Pounds per cubic foot
36+50...	4 1/2	134.1
	9	129.4
40+50...	4 1/2	138.5
	9	134.2
44+50...	4 1/2	133.7
	9	130.6

These results show that the density of the upper half of the compacted stabilized base was about 103 percent

of the density of the full 9 inches. On this basis the average density of 134 pounds per cubic foot for the 9-inch thickness indicates a density of 138 pounds per cubic foot in the upper 4½ inches. Assuming that the density for the 9-inch thickness is equal to the average of the densities of the upper and lower 4½ inches, the density of the lower 4½ inches may be calculated by multiplying the density of the 9-inch thickness by 2 and subtracting the density of the upper 4½ inches. The values obtained in this manner for stations 36+50, 40+50 and 44+50 are respectively 124.7, 129.9 and 127.5 pounds per cubic foot which correspond to densities averaging 94 percent of the densities of the upper 4½ inches and 97 percent of the densities of the full 9 inches.

The moisture contents of the base course, determined as a part of the density test, varied from 2.3 to 7.2 percent with an average of 4.4 percent.

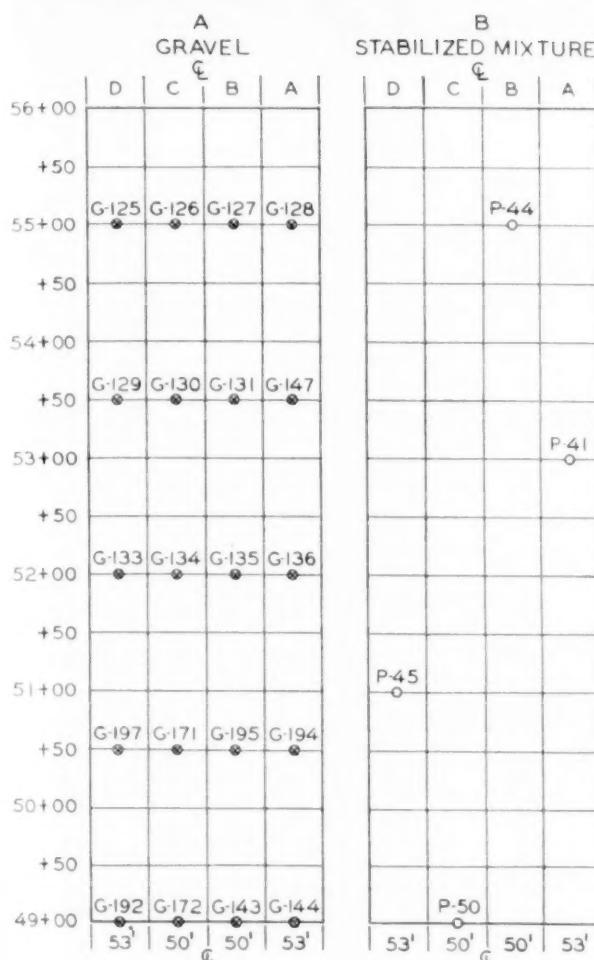


FIGURE 14.—PLAN OF LOCATIONS AT WHICH VARIOUS SAMPLES WERE TAKEN.

Tests made at three different locations on the North-South runway disclosed an average density of 125 pounds per cubic foot after four trips with the pneumatic-tired roller. After two trips with the three-wheel roller, the average density was increased to 128.7 pounds per cubic foot, and two additional trips increased it to 133.3 pounds per cubic foot.

#### SAMPLING AND TESTING PROCEDURES DESCRIBED

Sampling of the gravel consisted of digging a hole 12 inches deep in the graded runway after the oversize stone had been removed and collecting approximately 15 pounds of material from the sides of the hole. The runways were divided into strips 50 or 53 feet wide and samples were taken from each strip at intervals of 150 feet as illustrated in figure 14. The samples were placed in dust-tight canvas bags and delivered to the portable field laboratory which was located as close as possible to the section of the runway under construction.

The sample was first dried in shallow pans over a gasoline camp stove (fig. 15-A); it was stirred continuously to prevent burning. After the dried sample had cooled off, it was quartered down to about 4 pounds, placed in a pan, and ground with a rubber-covered pestle to break up the aggregation of particles. Any fine material having a tendency to adhere to the coarse gravel was removed with a wire brush. All of the



FIGURE 15.—LABORATORY TESTS ON SAMPLES. A, DRYING GRAVEL SAMPLES ON DOUBLE-BURNER GASOLINE CAMP STOVES; AND B, DETERMINING WEIGHTS OF MATERIAL RETAINED ON VARIOUS SIEVES.

material was then shaken through a nest of sieves ranging in size from the maximum to the minimum called for in the gradation requirements for the stabilized mixtures. The fraction retained on each sieve added to that retained on the sieves with larger openings was weighed (fig. 15-B) and the percentage of the total sample retained on each sieve was calculated. The form used for recording the data is shown in figure 16.

At the start of the work, samples of binder soil were obtained from the pit. After the hauling was commenced, samples were taken from the soil deposited on the runways. These samples were tested for moisture content as well as gradation, which was determined in the same manner as for the gravel.

One sample of the stabilized mixture was taken for each 200 lineal feet of runway as shown in figure 14-B. Some of these samples were tested in the portable field laboratory. The majority, however, were sent to the Public Roads Administration laboratory where their gradations, liquid limits, and plasticity indexes were determined in accordance with the standard methods of the American Association of State Highway Officials.

In practically all cases, the gravel required the addition of binder soil in order to provide a stable mixture. It was found that with the materials available best results were obtained with a mixture having approximately 7 or 8 percent passing the No. 200 sieve for the B, C, and D gradings and about 10 or 11 percent for the E grading. Tests performed on the mixtures showed that the liquid limit and plasticity index requirements could be satisfied with any acceptable gradation resulting from the combination of the existing gravel with the binder soils used on this project.

This simplified the proportioning to the considera-

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PUBLIC ROADS ADMINISTRATION  
Washington, D. C.

Sieve Analyses Record - Washington National Airport

Sample No. G-127 Date 5-9-40  
 Station 55+00  
 Location B Lane  
North - South Runway  
 : Retained : : Variation  
 : : : Passing:from grad-  
 Sieve :Weight:Percent:Percent:ing limits  
 :grams : : : Type.....  
 : : : : :  
 3 in. ....:.....:.....:  
 2 in. ....:.....:100:  
 1 in. ....:142....:11....:89....:  
 3/4 in. ....:263....:20....:80....:  
 3/8 in. ....:528....:39....:61....:  
 No. 4 ....:757....:56....:44....:  
 No. 10 ....:885....:66....:34....:  
 No. 40 ....:1097....:82....:18....:  
 No. 200 ....:1318....:98....:2....:  
 Passing No. 200 sieve .....:27..... grams  
 Wt. of total sample .....:1345..... grams  
 Tested by.....K..... Checked by.....T.....

Sample No. \_\_\_\_\_ Date \_\_\_\_\_  
 Station \_\_\_\_\_  
 Location \_\_\_\_\_  
 : Retained : : Variation  
 : : : from grad-  
 Sieve :Weight:Percent:Passing:ing limits  
 :grams : : Percent:Type.....  
 : : : : :  
 3 in. ....:.....:.....:  
 2 in. ....:.....:.....:  
 1 in. ....:.....:.....:  
 3/4 in. ....:.....:.....:  
 3/8 in. ....:.....:.....:  
 No. 4 ....:.....:.....:  
 No. 10 ....:.....:.....:  
 No. 40 ....:.....:.....:  
 No. 200 ....:.....:.....:  
 Passing No. 200 sieve .....:..... grams  
 Wt. of total sample .....:..... grams  
 Tested by ..... Checked by.....

Sample No. \_\_\_\_\_ Date \_\_\_\_\_  
 Station \_\_\_\_\_  
 Location \_\_\_\_\_  
 : Retained : : Variation  
 : : : Passing:from grad-  
 Sieve :Weight:Percent:Percent:ing limits  
 :grams : : : Type.....  
 : : : : :  
 3 in. ....:.....:.....:  
 2 in. ....:.....:.....:  
 1 in. ....:.....:.....:  
 3/4 in. ....:.....:.....:  
 3/8 in. ....:.....:.....:  
 No. 4 ....:.....:.....:  
 No. 10 ....:.....:.....:  
 No. 40 ....:.....:.....:  
 No. 200 ....:.....:.....:  
 Passing No. 200 sieve .....:..... grams  
 Wt. of total sample .....:..... grams  
 Tested by ..... Checked by .....

Sample No. \_\_\_\_\_ Date \_\_\_\_\_  
 Station \_\_\_\_\_  
 Location \_\_\_\_\_  
 : Retained : : Variation  
 : : : from grad-  
 Sieve :Weight:Percent:Passing:ing limits  
 :grams : : Percent:Type.....  
 : : : : :  
 3 in. ....:.....:.....:  
 2 in. ....:.....:.....:  
 1 in. ....:.....:.....:  
 3/4 in. ....:.....:.....:  
 3/8 in. ....:.....:.....:  
 No. 4 ....:.....:.....:  
 No. 10 ....:.....:.....:  
 No. 40 ....:.....:.....:  
 No. 200 ....:.....:.....:  
 Passing No. 200 sieve .....:..... grams  
 Wt. of total sample .....:..... grams  
 Tested by ..... Checked by .....

FIGURE 16.—FORM USED FOR RECORDING SIEVE ANALYSES.

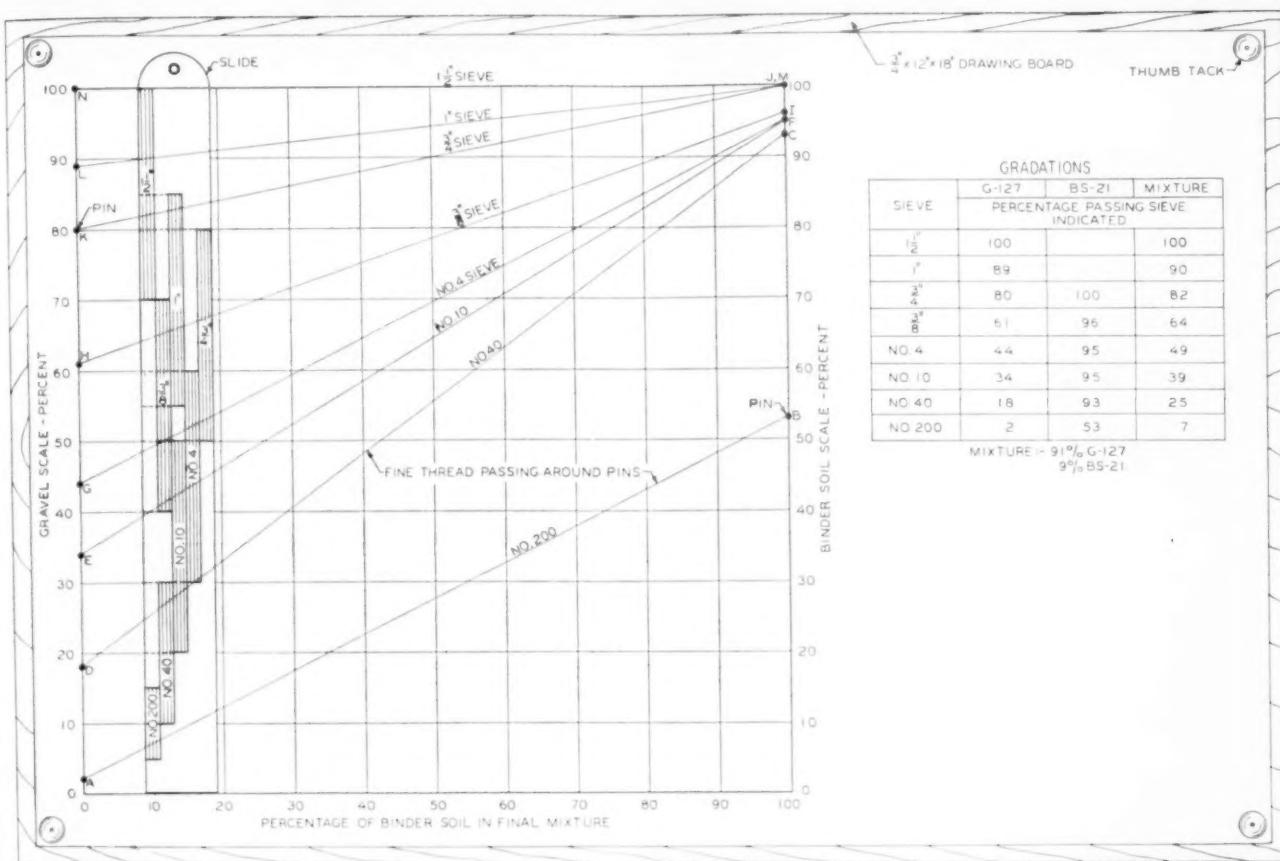


FIGURE 17.—GRAPHICAL METHOD FOR PROPORTIONING TWO SOIL MATERIALS TO PRODUCE SPECIFIED GRADING OF STABILIZED MIXTURE.

tion of grading alone. On the basis of their gradations, the proper proportions of the two materials, gravel and binder soil, were determined by either the trial-and-error method or the graphical method. The trial-and-error method consisted of assuming a certain percentage of binder soil to add to the gravel and calculating what the resulting mixture would be. If this assumed percentage did not prove satisfactory other percentages were tried until the calculations indicated a suitable mixture. After a little experience with the available materials, the desired combination could be obtained on the first trial.

The proportioning of the materials by the graphical method was performed using the mechanical device illustrated in figure 17. This consisted of a 12- by 18-inch drawing board on which was mounted a piece of cross section paper at least 10 inches long by 10 inches wide and having 10 divisions to the inch in each direction, a movable paper scale, several pins (represented by the small circles on the figure), and a fine thread looped around the pins. The fine thread is represented in figure 17 by the lines connecting the pins and having sieve designations.

#### GRAPHICAL METHOD USED IN PROPORTIONING MIXTURE

The movable scale is a strip of cross section paper having the same vertical scale as the fixed sheet. The limits of the specified grading are blocked off on this scale. A different movable scale had to be made for each grading band.

The operation of this device may best be illustrated by an example. For convenience in following the

procedure, the sieve analyses of gravel sample 127 (G-127) and binder soil sample 21 (BS-21) which are to be combined are shown on figure 17. The first step is to place pins along the vertical scales of the fixed sheet at points corresponding to the percentages passing the various sieves, on the left for the gravel and on the right for the binder soil. Next, the end of the fine thread is tied to pin A marking the percentage of gravel passing the No. 200 sieve (2 percent) and stretched across to pin B designating the percentage of binder soil passing the same sieve (53 percent). The thread is then extended straight up along the binder soil scale to pin C, across to pin D, up along the gravel scale to pin E, across to pin F, and so on to pins G, H, I, J, K, L, M, and ending at pin N.

The movable scale is placed under the threads along the pins on the left side and then moved to the right until the line (indicated by the left edge of movable scale) is reached where the greatest number of threads are crossing within the limits specified for the corresponding sieve sizes marked on the scale. The intersection of this line with the horizontal scale at the bottom of the sheet indicates the percentage of binder soil to be added to the particular sample of gravel, while the gradation of the mixture produced by this combination is read on the vertical scale at the points where this line intersects the lines formed by the different segments of the thread running across the sheet between the pins.

The calculation of the binder soil distribution was based on (1) the compacted dry density of the stabilized base assumed for design purposes as 135 pounds per

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PUBLIC ROADS ADMINISTRATION  
Washington, D.C.

Binder Soil Distribution Calculation - Washington National Airport

**Design data:**

Compacted weight of stabilized mixture (lbs. per cu. ft.)	135	Computed by.....	K.....
Thickness stabilized (inches)	9	Checked by.....	T.....
Compacted weight of stabilized mixture (lbs. per sq. yd.)	911	Date .....	5-9-40.....

	R.R.	R.R.	R.R.	R.R.	:	:	:
<u>Binder soil pit</u>							
<u>Binder soil type</u>	BS-21	BS-21	BS-21	BS-21			
<u>Moisture content (percent)</u>	8	12	8	8			
<u>Binder soil required (percent)</u>	4	6	9	9			
<u>Binder soil per load (lbs.)</u>	4870	4870	4870	4870			
<u>Dry binder soil required (lbs. per sq. yd.)</u>	36	55	82	82			
<u>Moist binder soil required (lbs. per sq. yd.)</u>	39	59	89	89			
<u>Distribution (sq. yds. per load)</u>	125	83	55	55			
<u>Width of spread (ft.)</u>	26 <sup>1</sup>	25	25	25			
<u>Lineal distance per load (ft.)</u>	42	29	20	20			
<u>Gravel samples represented</u>	125	126	127	131			

R.R. denotes Roaches Run

FIGURE 18.—FORM USED FOR CALCULATION OF BINDER SOIL DISTRIBUTION.

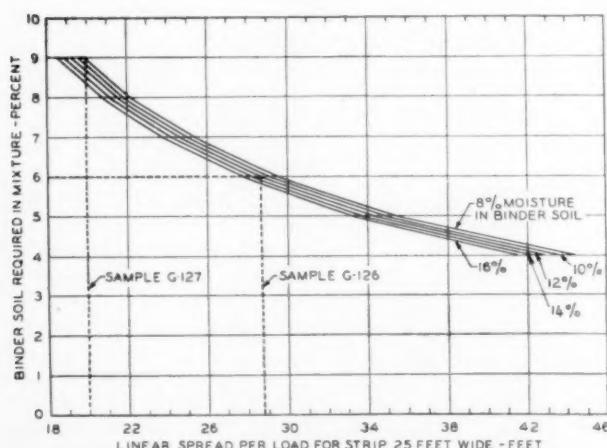


FIGURE 19.—GRAPHICAL DETERMINATION OF BINDER SOIL DISTRIBUTION

cubic foot, (2) the moisture content of the soil as determined in the laboratory, (3) the percentage of binder soil in the mixture determined as described above, and (4) the weight of soil contained in the 2-cubic yard transportable box which was found to average 4,870 pounds. The variation in weight of any individual load from the average was negligible in amount.

The form used for the calculation is illustrated in figure 18. On the basis of a dry density of 135 pounds

per cubic foot, the weight of dry materials in 1 square yard of compacted stabilized base, 9 inches thick, equals 911 pounds. The amount of dry binder soil in pounds per square yard to be spread on the runway is equal to 911 multiplied by the percentage of binder soil in the mixture divided by 100. In the case of gravel sample 127 and binder soil sample 21, for

example, this amounts to  $\frac{911 \times 9}{100}$  or 82 pounds. Cor-

recting for a moisture content of 8 percent, this value becomes  $82 \times 1.08$  or 89 pounds of moist binder soil per square yard. Dividing the weight of a load of binder soil (4,870 pounds) by 89 gives 55 square yards as the area covered by one load of binder soil.

For convenience in spreading by hand, the width of spread for each load was fixed at a maximum of 25 feet for the inside 50-foot strips of the runways and 26<sup>1</sup>/<sub>2</sub> feet for the outside strips 53 feet wide. The linear distance in feet per load was computed for the corresponding width.

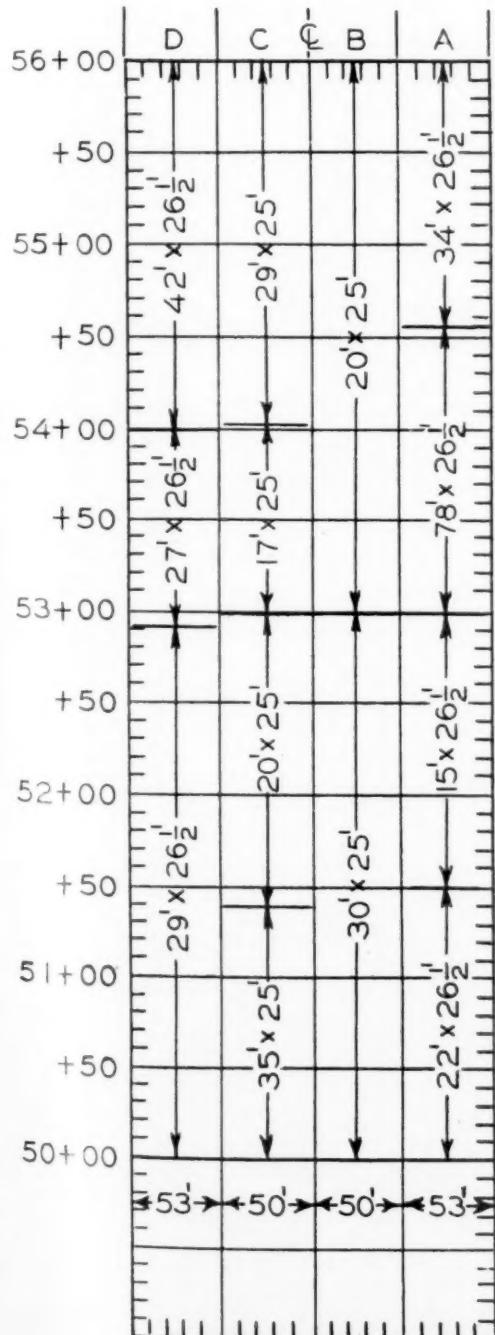
It will be seen from the above calculation that for a given width of spread the linear distance per load depends on the percentage of binder soil in the mixture and the moisture content of the binder soil. Accordingly charts were constructed from which the distribution of the binder soil was determined graphically. The chart used when the width of spread was 25 feet is shown in figure 19.

FEDERAL WORKS AGENCY  
PUBLIC ROADS ADMINISTRATION  
Washington, D.C.

Stabilization Record - Washington National Airport

Location NORTH - SOUTH RUNWAY

Date MAY 9, 1940



To - Superintendent of Stabilization  
From - Inspector (P.R.A.)

Subject - Binder soil distribution.

The area indicated on sketch by .....  
..... is in condition to receive  
binder soil type BS-2J from pit located in  
upland area ROACHES RUN.....  
and shall be distributed as follows:

Sta. to	Sta.	Strip	Quantity in lbs. per sq.yd.	Lineal feet per load for width of 25 & 26 1/2
50+00	56+00	ABCD	VARIABLE	SEE SKETCH

FIGURE 20.—INSTRUCTION SHEET FOR DISTRIBUTION OF BINDER SOIL.

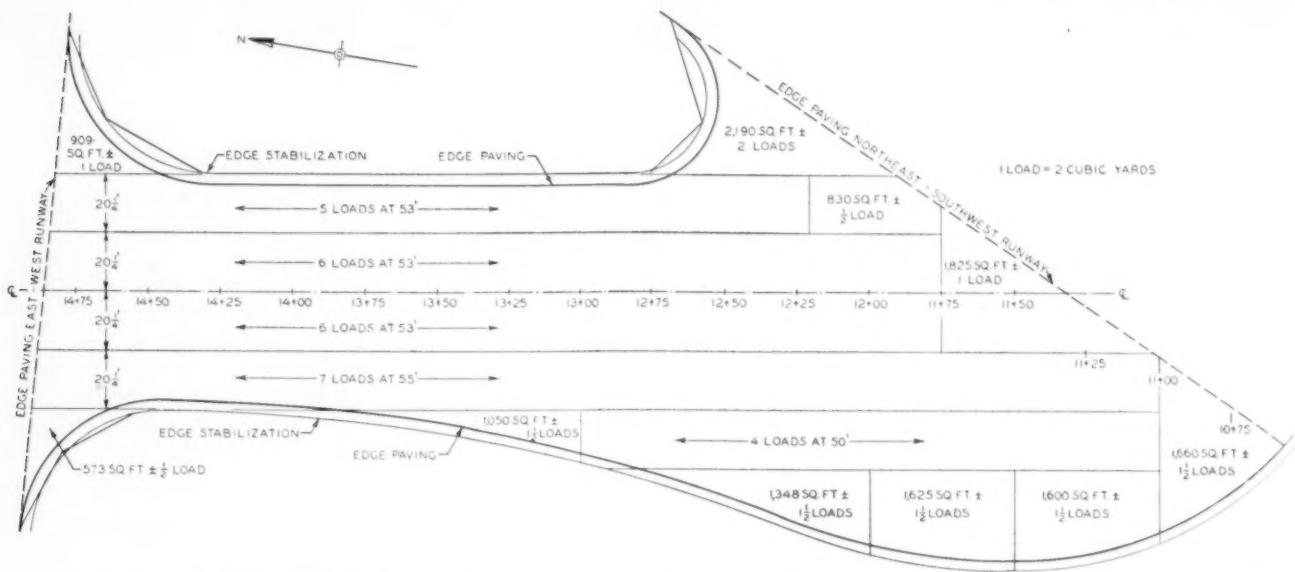


FIGURE 21.—BINDER SOIL DISTRIBUTION SHEET FOR TAXISTRIP NO. 6, SECTION 1.

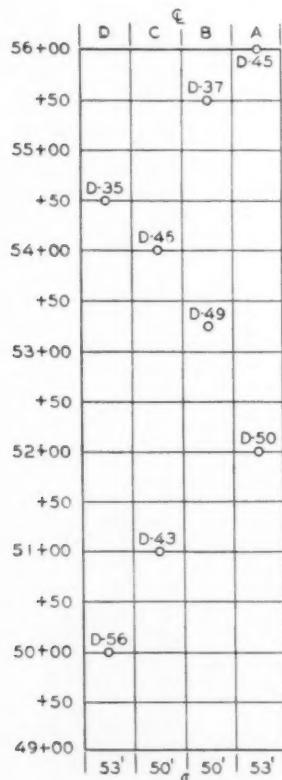


FIGURE 22.—PLAN OF LOCATIONS AT WHICH DENSITY SAMPLES WERE TAKEN.

Figure 20 is an example of the sheet furnished to the superintendent of stabilization showing the dimensions of the area for each load of binder soil to be placed on different parts of the runway. In runway or taxiway sections of irregular shape, a binder soil distribution sheet such as that shown in figure 21 was issued to the superintendent. Under these conditions, the application of binder soil was made to the nearest  $\frac{1}{2}$  load or 1 cubic yard.

#### MOTOR OIL USED IN DENSITY DETERMINATIONS

The locations where density tests were made depended on the order in which different areas were completed. A typical pattern is shown in figure 22. The test procedure used on this project was as follows:

A soil collecting tray, 15 inches square, having a  $4\frac{1}{2}$ -inch circular opening in the center was set in place on the leveled surface (fig. 23-A) and a hole was dug through the compacted base by loosening the material with a trowel or pointed bar. The loosened material was scooped out with a large spoon, placed in a pail, and weighed on a spring scale of 30 pounds capacity (fig. 23-B). The indicator on the scale was adjusted for the weight of the pail so that the weight of the material removed from the hole was read directly. The moisture content of this material was then determined in the laboratory.

The circular opening in the tray served as a template for digging the hole while the tray itself collected the loosened material which tended to scatter during the digging, together with any that might have spilled from the spoon in transferring the material from the hole to the pail.

After all the loosened material had been removed, the hole was filled with motor oil (S. A. E. 40) from a 3-gallon can (fig. 23-C) and the can plus the oil remaining in it after filling the hole was weighed (fig. 24). The weight of the can plus the original volume of oil had been previously determined. The difference between the two weights gave the weight of oil in the hole. A hand suction pump was used to remove the oil from the hole.

The volume of the hole was then determined by dividing the weight of the oil in the hole by the known weight of 56 pounds per cubic foot of oil.

The density of the base course in pounds per cubic foot as compacted in the moist condition was calculated by the formula:

$$\text{Wet density} = \frac{\text{weight of moist material removed from hole}}{\text{volume of hole}}$$

(Continued on p. 191)

# LIGNIN BINDER USED IN TEST SECTIONS SUBJECTED TO ACCELERATED TRAFFIC

BY THE DIVISION OF TESTS, PUBLIC ROADS ADMINISTRATION

Reported by EDWARD A. WILLIS, Associate Highway Engineer, and RICHARD C. LINDBERG, Junior Highway Engineer

**L**IGNIN BINDER, a by-product in the manufacture of paper from wood by the sulfite process, has been used, at least experimentally, in road construction for many years.<sup>1</sup> Since 1936, this sulfite liquor, marketed under a trade name, has been used by several of the State highway departments for the treatment of gravel surfaces and base courses.

This report is the fifth in a series describing investigations of materials for surface and base course construction. Former reports discussed laboratory tests and accelerated tests on a circular track of sand-clay, sand-clay-gravel, nonplastic granular materials with admixtures of water-retentive chemicals, and chert-gravel.

The present report describes similar investigations in which crusher-run materials—limestone, granite, slag, and gravel—were mixed with a binder-soil and tested in an outdoor circular track.

The circular track used in these investigations was the same as that used in the studies of water-retentive chemicals as admixtures with nonplastic roadbuilding materials, which have been reported previously.<sup>2</sup> The tire equipment was 30 inches by 5 inches of the high-pressure type inflated to a pressure of 80 pounds per square inch. The load on each wheel was 800 pounds during the entire test.

Distributed traffic was obtained by means of a mechanical device which gradually shifted the rotating beam with respect to its axis of rotation. Concentrated traffic was used in testing the materials after the surface treatment had been constructed. This was obtained by locking the sliding pivot of the beam in such a position that the wheels pursued two concentric circular courses having centerlines about  $2\frac{1}{2}$  inches on each side of the centerlines of the test sections.

## SIX SECTIONS TESTED IN CIRCULAR TRACK

Six sections were tested in this investigation. Each section was 18 inches wide, 6 inches deep, and approximately 6.3 feet long. All the test sections were laid over a porous, crushed-stone subbase through which water introduced from below could pass.

<sup>1</sup> Dust Preventives and Road Binders, by Prevost Hubbard. John Wiley and Sons, New York, 1910.

<sup>2</sup> Studies of Water-Retentive Chemicals as Admixtures with Nonplastic Road-Building Materials, by E. A. Willis and C. A. Carpenter, PUBLIC ROADS, vol. 20, No. 9, Nov. 1939.

An investigation is reported in which crusher-run limestone, granite, slag, and gravel were mixed with a binder soil and tested in an outdoor circular track. The mixtures were first tested without any form of surface application. They were then treated with lignin binder and the tests continued. Finally, they were tested as base courses under a thin bituminous surface treatment.

Tests with distributed traffic prior to the application of lignin binder showed that an admixture of 10 percent of hydrated lime, which was present in two sections, improved the performance of both the granite-soil mixture and the gravel-soil mixture as surface courses. Under the same test conditions, the other four sections which had no chemical admixture showed signs of raveling under prolonged traffic.

The application of lignin binder at the rate of  $\frac{1}{2}$  gallon per square yard tended to cause softening and instability for a time. This condition gradually improved as traffic was continued. Thereafter the sections remained stable; and although the lignin did not prevent raveling, it did retard raveling as compared with tests on the untreated sections.

All sections gave good performance when tested under normal conditions of moisture as base courses for a thin bituminous surface treatment. Under extreme conditions the two sections containing granite became unstable. The lignin binder which was present while the materials were being tested as base courses did not alter the performance, either adversely or beneficially, from that which was anticipated from laboratory tests prior to the addition of the lignin binder.

Three different kinds of crusher-run aggregate (limestone, slag, granite) and crushed Potowmack River gravel were used as coarse material in the test sections. The binder soil used was a local clay having a liquid limit of 41 and a plasticity index of 18. Two of the sections, Nos. 5 and 6, had 10 percent by weight of hydrated lime combined with the soil-aggregate mixtures.

The compositions of the six sections are shown in table 1. Thus, for example, section 1 contained 90 percent by weight of limestone screenings and 10 percent by weight of binder soil. Section 5 was identical with section 2 except for the admixture of 10 percent by weight of hydrated lime, and section 6 was like section 4 except for the addition of 10 percent of hydrated lime.

The gradings and soil constants of the mixtures used are given in table 2. The effect of the hydrated lime admixture in increasing

TABLE 1.—Composition of sections

Section No.	1	2	3	4	5	6
Granite.....	Percent <sup>1</sup> 90	Percent <sup>1</sup> 92	Percent <sup>1</sup> 80	Percent <sup>1</sup>	Percent <sup>1</sup> 92	Percent <sup>1</sup>
Slag.....						
Limestone.....	90					
Gravel.....						
Binder soil.....	10	8	20	15	8	85
Total.....	100	100	100	100	100	100
Hydrated lime.....					10	10

<sup>1</sup> Percentage based on dry weight.

TABLE 2.—Gradings and soil constants of mixtures used in the track

Section No.	1	2	3	4	5	6
Grading:	Percent	Percent	Percent	Percent	Percent	Percent
Passing $\frac{3}{4}$ -inch sieve.....	100	100	100	100	100	100
Passing $\frac{3}{8}$ -inch sieve.....	100	100	98	94	100	94
Passing No. 4 sieve.....	98	98	78	70	96	72
Passing No. 10 sieve.....	65	69	54	56	68	52
Passing No. 40 sieve.....	34	48	37	38	46	35
Passing No. 200 sieve.....	21	22	23	19	22	17
Dust Ratio <sup>1</sup> .....	62	46	62	50	48	49
Tests on material passing No. 40 sieve:						
Liquid limit.....	19	24	25	20	29	27
Plasticity index.....	5	2	7	5	2	5

<sup>1</sup> Dust ratio =  $100 \times \frac{\text{Percentage passing No. 200 sieve}}{\text{Percentage passing No. 40 sieve}}$ .

the liquid limit can be seen by comparing the analysis of section 5 with that of section 2 and section 6 with that of section 4.

The circular track tests were divided into three parts. The mixtures were first tested without any form of surface application. They were then treated with lignin binder and the tests continued. Finally, they were tested as base courses under a thin bituminous surface treatment.

The procedure for preparing the materials for the track tests, constructing the test sections, applying waste sulfite liquor, and surface treating, was as follows:

1. The aggregates were proportioned by weight from stock piles and were thoroughly mixed before any water was added.

2. Hydrated lime was added to the materials for sections 5 and 6 and thoroughly mixed before wetting.

3. Water was then added in amount sufficient to cause the mixture to make a firm ball when squeezed in the hand and mixing continued to distribute the moisture uniformly.

4. The moistened mixtures were placed in the trough of the track in two approximately equal layers, each layer being compacted with pneumatic-tired traffic uniformly distributed over the surface. Material was added to the top lift of each section as compaction took place until the surface of the base course was from  $\frac{1}{2}$  inch to 1 inch below the curbs.

5. Compaction with distributed traffic was continued on the top layer for 40,000 wheel-trips. At this time all of the sections showed some corrugation and raveling. Section 3 had only a slight amount of corrugation and section 6 had the least of all.

6. The sections were trimmed smooth to a level 1 inch below the top of the curbs. It was necessary to add more material to sections 1 and 4 to bring them up to the desired level. This was done by lightly scarifying the compacted surface, placing additional material and hand tamping. Two thousand six hundred wheel-trips of distributed traffic were used to compact this material.

7. The sections were then tested without any form of surface treatment but with different ground water elevations; 160,000 wheel-trips of distributed traffic were applied to the materials in this first phase of the testing.

8. An application of a commercial grade of waste sulfite liquor at the rate of  $\frac{1}{2}$  gallon per square yard was made on the reshaped sections at the conclusion of the previous part of the test. The liquor contained 46 percent solids as received and was diluted with an equal part of water before it was applied.

9. After application of the waste sulfite liquor and compaction by 6,200 wheel-trips of distributed traffic, 100,000 wheel-trips of distributed traffic were applied, with different ground water elevations. This comprised the second phase of the testing procedure.

10. High places in the sections were leveled off and all loose material was removed preparatory to the application of a surface treatment.

11. A light tar prime was applied at the rate of 0.2 gallon per square yard and allowed to cure.

12. A surface treatment of 0.4 gallon of hot application bituminous material and a cover of 50 pounds per square yard of  $\frac{3}{4}$ -inch maximum size stone was applied.

13. The treatment was consolidated by additional distributed traffic until the surface was well sealed and showed no movement.

14. Concentrated traffic in the amount of 160,000 wheel-trips was then applied while the water elevation in the trough was varied. This was the third and final phase of circular track tests.

#### BEHAVIOR OF TEST SECTIONS JUDGED BY APPEARANCE AND DISPLACEMENT

The behavior of the materials being investigated was judged on the basis of the appearance of the sections at various stages of the tests, supplemented by measurements of vertical displacements of the surface. The measurements were made with the transverse<sup>3</sup> and longitudinal<sup>4</sup> profilometers which have been described in previous reports.

The schedule of traffic applications and changes in water elevation with notations on the behavior of the six test sections are shown in table 3. The average vertical displacements measured by the transverse and longitudinal profilometers are shown in figures 1 and 2. Initial profile measurements were taken at the beginning of each of the three phases of testing after apparently complete compaction by distributed traffic had been obtained. Changes in the behavior of the various sections under altered test conditions are shown by changes in the slopes of the displacement curves.

All of the sections compacted well initially. At the conclusion of the first compaction period (42,600 wheel-trips) water was admitted until its level was 1 inch above the top of the subbase. Initial profiles were taken at this time and traffic resumed. Less than 3,000 wheel-trips of traffic caused section 2, composed of granite and soil, to become soft and unstable. The section was consequently reshaped, tamped, and sprinkled but little benefit was noted. From time to time it was necessary to add to section 2 to replace material pushed over the curbs.

At this time the other sections were in good condition. At 70,000 wheel-trips section 5, which was similar to section 2 except for the addition of hydrated lime, began to develop a soft spot which later (82,600 wheel-trips) had to be filled with additional material. At 80,000 wheel-trips section 3, composed of slag and binder soil, began to shave but this condition had ceased by the time profiles were taken at 82,600 wheel-trips. So much raveling and movement had taken place in section 2 that the profile trace would not fall upon the profile paper used in the measurements of displacement. Sections 3 and 5 had also worn so badly it was necessary to add material to them. The remaining sections were in good condition at this time.

Traffic was continued under the same conditions for an additional 20,000 wheel-trips. Section 2 required sprinkling to keep the surface knit together, and it was necessary to rake material from the curbs to the center of the section. This was also necessary in section 3 where it adjoined section 2. Profiles were taken at 102,600 wheel-trips, or at the end of 60,000 wheel-trips with water 1 inch above the top of the subbase. Profiles taken at this time of sections 2, 3, and 5 were not truly representative of actual wear and displacement because of the material added to prevent jarring of the beam.

Distributed traffic was continued with the water level 1 inch below the top of the subbase. Section 2 improved somewhat during this time as regards stability

<sup>3</sup> Circular Track Tests on Low-Cost Bituminous Mixtures, by C. A. Carpenter and J. F. Goode, PUBLIC ROADS, vol. 17, No. 4, June 1936.

<sup>4</sup> A Study of Sand-Clay-Gravel Materials for Base Course Construction, by C. A. Carpenter and E. A. Willis, PUBLIC ROADS, vol. 20, No. 1, March 1939.

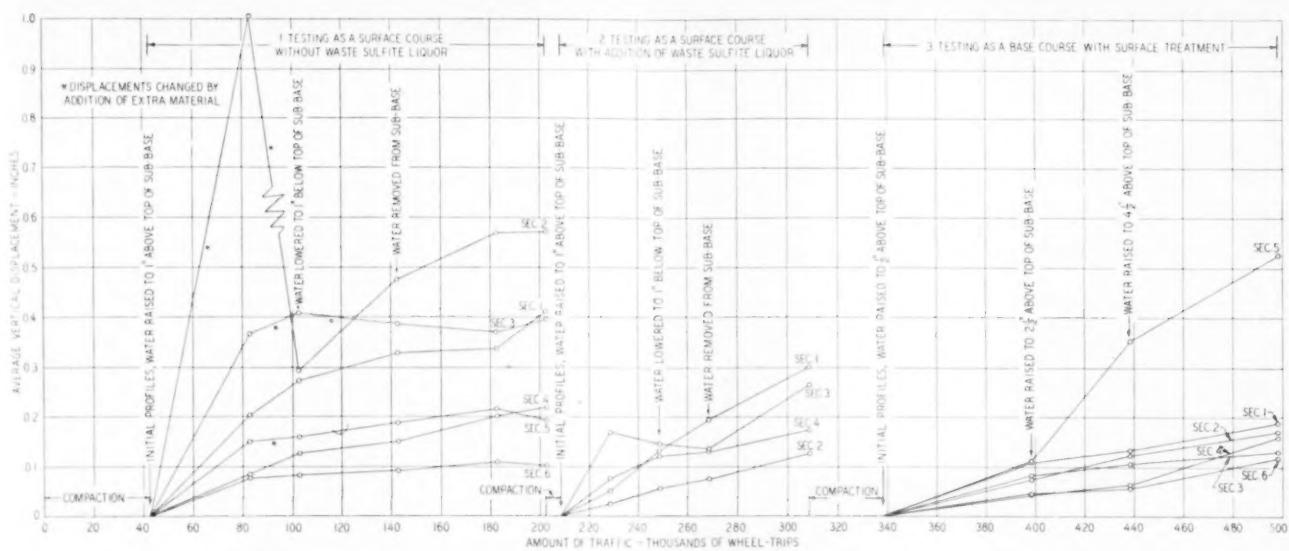


FIGURE 1.—RATE OF SURFACE DISPLACEMENT, TRANSVERSE MEASUREMENTS.

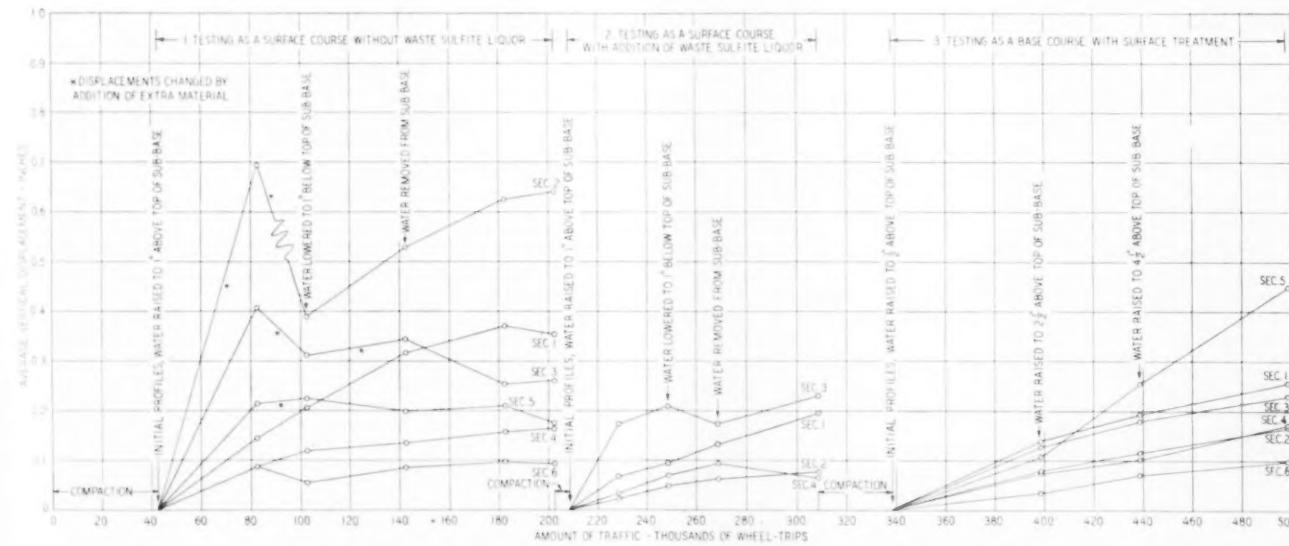


FIGURE 2.—RATE OF SURFACE DISPLACEMENT, LONGITUDINAL MEASUREMENTS.

but raveling of the surface was observed. When profiles were taken at 142,600 wheel-trips, sections 2 and 3 showed the most displacement and sections 4 and 6 the least.

Distributed traffic was continued with the water completely removed from the subbase. During the testing period, from 142,600 to 202,600 wheel-trips, there was a general improvement in the appearance of all the sections although the displacement as measured by the profilometers continued to increase with few exceptions.

Visual inspection and the profiles showed that section 2 had suffered the greatest displacement and wear, much loose material being present on the surface. Section 1, consisting of limestone and binder soil, showed some corrugation but underneath the loose surface the material was well knit together. Sections 3 and 4, composed of slag and binder soil and gravel and binder soil, respectively, were not unduly loose on the surface. Sections 5 and 6, both of which contained hydrated lime, were in the best condition.

The appearance of the sections after 202,600 wheel-trips is shown by the photographs in figure 3. Corrugations in section 1 are shown in figure 3-A; beneath the loose material the section was firm. The extremely loose condition of the surface of section 2 is shown in figure 3-B. The condition of sections 3 and 4 at the end of this phase of the testing is illustrated by figure 3-C. Figure 3-D shows section 6 and is representative of both sections 5 and 6. This photograph shows the hard, plaster-like appearance of the surface in many parts of these two sections which had been treated with hydrated lime. Loose material had been swept away from a part of the surface shown near the center of the photograph.

#### WASTE SULFITE LIQUOR APPLIED AS SURFACE TREATMENT

In the second phase of the tests (see table 3) waste sulfite liquor was applied to the surface of the sections at the rate of  $\frac{1}{2}$  gallon per square yard. Testing with distributed traffic was then continued.

TABLE 3.—*Schedule of operations and behavior of test sections*

Operation	Traffic	Water level above top of sub-base	Behavior					
			Section 1	Section 2	Section 3	Section 4	Section 5	Section 6
Placing and compacting	Wheels trips 0-1 42,600 42,600- 82,600	Inches <sup>1</sup> 0 1	Raveling Good	Some raveling Unstable <sup>4</sup>	Some raveling Slightly unstable	Raveling Good	Some raveling Slightly unstable	Good, Do.
1. Testing as surface course, without waste sulfite liquor	82,600- 102,600 Do 102,600- 142,600 Do 142,600- 182,600 Do 182,600- 202,600 Compaction of surface after treatment with waste sulfite liquor	1 <sup>3</sup> -1 <sup>2</sup> 0 <sup>2</sup> 0 202,600- 208,800	do Some raveling Raveling do Good	Raveling <sup>4</sup> Some raveling Raveling do Good	Some raveling <sup>4</sup> do do do Unstable	Some raveling Good Some raveling do Good	Some raveling <sup>4</sup> Good Some raveling do do do Unstable	Do, Do, Do, Do, Unstable,
2. Testing as surface course with addition of waste sulfite liquor	208,800- 228,800 Do 228,800- 248,800 Do 248,800- 268,800 Do 268,800- 308,800 Compacting surface treatment	1 <sup>1</sup> -1 <sup>3</sup> -1 <sup>2</sup> 0 <sup>2</sup> 0 308,800- 338,800 338,800- 398,800	do Good do do Some raveling Good do	Slightly unstable <sup>4</sup> Good do Raveling Good do	do Good do Raveling Good do	Slightly unstable <sup>4</sup> do do do do do	do Good do do do do	Do, Good, Do, Do, Do, Do,
3. Testing with concentrated traffic as a base course, waste sulfite liquor still present	308,800- 438,800 Do 438,800- 498,800	<sup>2</sup> ½ <sup>4</sup> ½	do do	do do	do do	do do	Slightly unstable Failed	Do, Do.

<sup>1</sup> 2,600 wheel-trips to compact additional material in sections 1 and 4.<sup>2</sup> No water in subbase.<sup>3</sup> Water level 1 inch below top of subbase.<sup>4</sup> Necessary to add material to prevent jarring of the beam.<sup>5</sup> Unstable at start but gradually improved after scarifying during second phase of testing.

In applying the lignin binder, the sections first were scarified to about 2 inches below the curbs and more material was added until the loose material was about  $\frac{1}{2}$  inch above the curbs. After the sections had been lightly sprinkled, waste sulfite liquor was applied at the rate of  $\frac{1}{2}$  gallon per square yard to the loose, uncompacted material. The attempt to apply traffic was unsuccessful as the rubber-tired wheels picked up the material and whipped it away.

Failure of this attempt at compaction resulted in trial of other means. All material was removed down to where the base was solid and firm, and new material was added. This material was tamped into place, lightly sprinkled with water, and allowed to dry overnight. Two hundred wheel-trips were used to compact the surface. Then waste sulfite liquor was applied at the rate of  $\frac{1}{2}$  gallon per square yard. After 48 hours, the treatment appeared to have penetrated thoroughly. Places where there seemingly was an excess of sulfite liquor had a shiny, slick surface much like a road on which excess bituminous material had been used. Figure 4 shows the appearance of the surface after the application of the waste sulfite liquor.

The water level was raised to 1 inch above the top of the subbase and distributed traffic was then continued. Two thousand wheel-trips were at slow speed and the 4,000 wheel-trips at regular speed. The lignin binder which had failed to penetrate in section 5 adhered to the tires when they passed over and was removed from the surface in this manner. At these places, the compacted material underneath was quite moist with capillary water. Section 6 started to break up at 205,150 wheel-trips and it was necessary to scarify and allow the loosened material to dry before resuming traffic.

In section 5 wherever there was a skin of surplus liquor on the surface, the base beneath was very moist and the same scarifying treatment was given this section as well. Water was withdrawn from the subbase during the drying period. After drying, the material in both sections was replaced and tamped firmly. Section 3 was showing signs of movement at this time

but it was not deemed necessary to scarify this material.

At 208,800 wheel-trips, initial profiles for the second phase of the tests were taken of sections 1 to 4. Sections 5 and 6 were so unstable that no attempt was made to measure their displacements. Distributed traffic was continued. At 216,200 wheel-trips, section 4 developed a soft spot which increased in size. Sections 1, 2, and 3 were in good condition. Sections 5 and 6, which were unstable at the start of the second phase of testing, had improved and were very stable.

At 248,800 wheel-trips, the water level was dropped to 1 inch below the top of the subbase and traffic resumed. At this time all sections were in good condition. The waste sulfite liquor treatment had a tendency to scale off in sections 1 and 3. There appeared to be very little penetration of the material.

After withdrawal of water from the subbase at 268,800 wheel-trips distributed traffic was resumed. Sections 1, 2, and 3 showed signs of raveling, particularly section 3, at the completion of 40,000 wheel-trips without water in the subbase. The other three sections were in good condition.

At the conclusion of the second phase of the testing at 308,800 wheel-trips, all loose material was swept from the surface and all high places were leveled off. A light tar prime was applied at the rate of 0.2 gallon per square yard and a thin bituminous surface treatment consisting of 0.4 gallon of hot application bituminous material and 50 pounds of  $\frac{1}{4}$ -inch maximum size stone per square yard was constructed. Compaction of the surface treatment was accomplished with 30,000 wheel-trips of distributed traffic. Sections 5 and 6, which had been particularly unstable at the start of the previous phase of the investigation, were now tested as base courses without any changes in their composition.

The performance of the sections as bases is best shown by the displacement curves, figures 1 and 2. Section 5, composed of granite, soil, and hydrated lime, showed the greatest displacement of all the sections. It began to shove at about 418,800 wheel-trips with the water elevation at  $2\frac{1}{2}$  inches above the

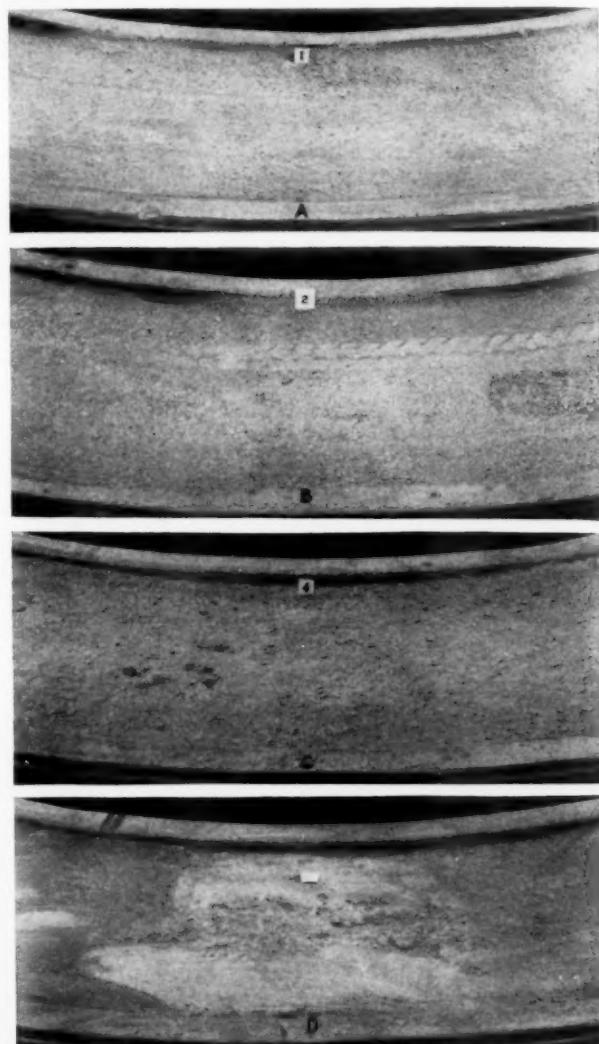


FIGURE 3.—APPEARANCE OF TEST SECTIONS AFTER 202,600 WHEEL-TRIPS OF DISTRIBUTED TRAFFIC ON THE UNTREATED MATERIAL. A, SECTION 1; B, SECTION 2; C, SECTION 4, WHICH IS ALSO REPRESENTATIVE OF THE APPEARANCE OF SECTION 3; AND D, SECTION 6, WHICH IS ALSO REPRESENTATIVE OF THE APPEARANCE OF SECTION 5.



FIGURE 4.—APPEARANCE OF TEST SECTIONS AFTER APPLICATION OF WASTE SULFITE LIQUOR. A, SECTIONS 1, 2, AND 3 (FROM LEFT TO RIGHT); and B, SECTIONS 4, 5, AND 6.

top of the subbase. At 498,800 wheel-trips (the end of the test) section 5 had completely failed. At this same time section 2, composed of granite and soil, was showing slightly under the wheels. Sections 1, 3, and 4 were in a satisfactory condition, and section 6, which

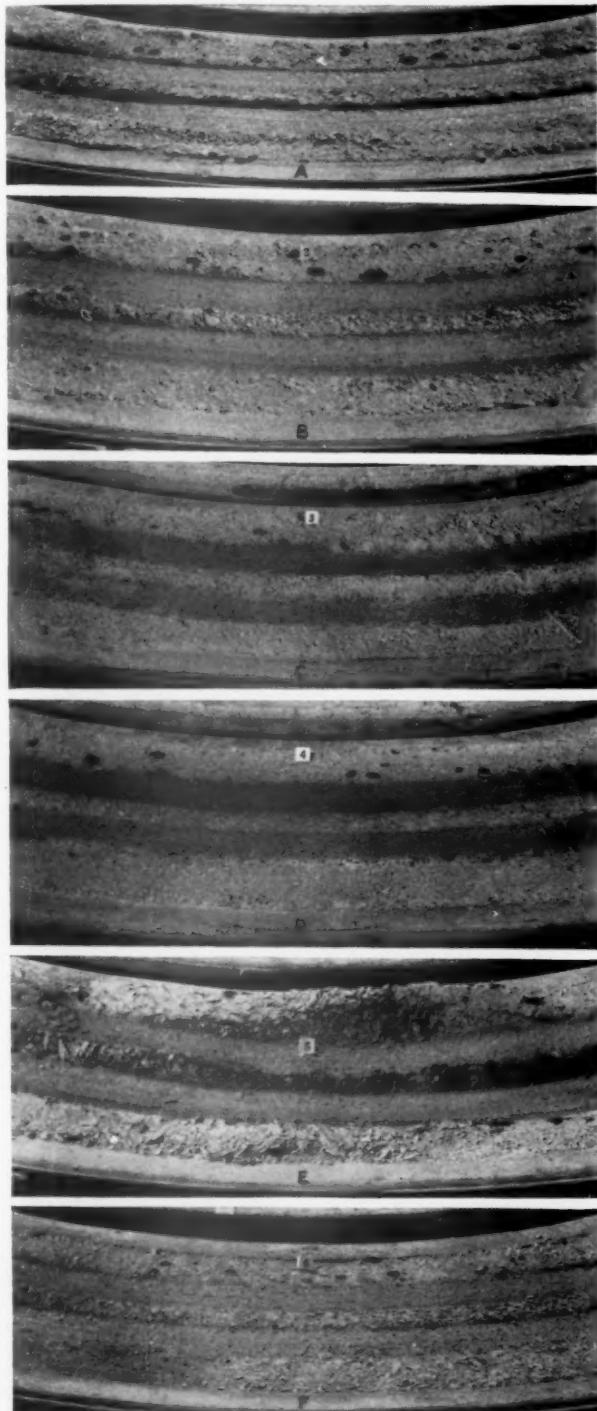


FIGURE 5.—APPEARANCE OF TEST SECTIONS AFTER 498,800 WHEEL-TRIPS. PICTURES A TO F CORRESPOND TO SECTIONS 1 TO 6, RESPECTIVELY.

had become unstable temporarily when tested with a treatment of waste sulfite liquor, was in the best condition of all the sections. Figure 5 shows the condition of the sections at the conclusion of the test.

At the conclusion of the track tests, samples were taken from each section for density and moisture content determinations. Table 4 shows the values obtained and also the volumetric composition of the samples.

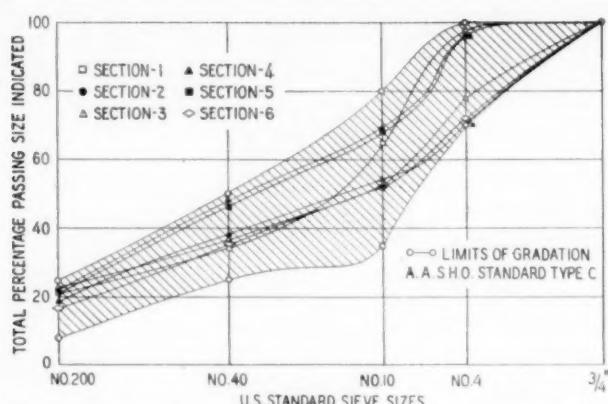


FIGURE 6.—GRADINGS OF MATERIALS USED IN TRACK TESTS.

The addition of hydrated lime reduced the density and also increased the moisture content of those mixtures in which it was present. Thus, the volumetric composition of section 2 was 81.9 percent solids, 10.9 percent water, and 7.2 percent air. The composition of section 5, which differed from section 2 only by the addition of 10 percent of hydrated lime, was 70.5 percent solids, 20.4 percent water, and 9.1 percent air. Similarly, section 4 had 83.3 percent solids while section 6, containing lime, had only 76.0 percent solids.

Section 1, consisting of limestone screenings and soil, had the highest density of any of the sections. The solids by volume of the sample from this section were 87.8 percent. Sections 2, 3, and 4 all had approximately the same density at the end of the test, as shown in table 4.

TABLE 4.—Density of specimens taken from track at end of test

Section No.	Density		Moisture	Composition by volume		
	Wet	Dry		Solids	Water	Air
1	Lb. per cu. ft. 151.2	Lb. per cu. ft. 145.2	Percent 4.1	Percent 87.8	Percent 6.5	Percent 5.7
2	144.7	135.5	6.8	81.9	10.9	7.2
3	146.2	134.1	9.0	81.1	14.4	4.5
4	145.0	137.8	5.2	83.3	8.3	8.4
5	131.3	116.5	12.7	70.5	20.4	9.1
6	139.6	125.7	11.1	76.0	17.8	6.2

## SUMMARY

The grading curves for the six combinations of materials tested are shown in figure 6. The shaded band in this figure is drawn to include the A. A. S. H. O. specification requirements for crusher-run (type C) surface-course materials. The grading requirements for the similar type of base-course materials are identical with those for surface courses.

The gradings of all the mixtures tested in the 6 sections of the track fall within the shaded band and, consequently, meet the grading requirements of the specifications.

The A. A. S. H. O. specifications for type C or crusher-run materials further stipulate that the fraction passing the No. 40 sieve shall have a liquid limit not greater than 35 and a plasticity index not less than 4 or more than 9 if the materials are to be used as surface courses, and that the same fraction shall have a liquid limit of not more than 25 and a plasticity index of not more than 3 if the materials are to be used as base courses. These specifications also state the ratio of the

fraction passing the No. 200 sieve to the fraction passing the No. 40 sieve shall be less than two-thirds for surface-course materials and less than one-half for base-course materials.

Consequently, sections 1, 3, 4, and 6 meet the requirements for surface-course materials only, the plasticity index being too high to conform to the specification limits for base course materials. Section 2 falls within the base but not the surface course requirements because it has a plasticity index of 2. Section 5 does not conform to the A. A. S. H. O. specifications for either base- or surface-course materials. The plasticity index of 2 is too low to meet the surface-course requirements and the liquid limit of 29 is too high to meet the base-course requirements.

*Performance as surface courses.*—The tests with distributed traffic prior to the application of lignin binder showed that the addition of 10 percent of hydrated lime improved the performance of both the granite-soil mixture (compare secs. 2 and 5) and the gravel-soil mixture (compare secs. 4 and 6) as surface courses.

Thus, the behavior of section 2, which was a mixture of 92 percent granite screenings and 8 percent binder-soil meeting the grading requirements but not the plasticity index requirements of the A. A. S. H. O., type C, surface-course material specifications, was definitely unsatisfactory throughout the first phase of the testing. The behavior of section 5, which differed in composition from section 2 only in the addition of 10 percent of hydrated lime, while inferior to some of the sections, was considerably better than that of section 2.

The gradings of the mixtures used in the two sections were almost identical and both had a plasticity index of 2. The appearance of the two sections after 202,600 wheel-trips and just before the application of the lignin binder is illustrated by figures 3-B and 3-D.

Section 4, consisting of a mixture of 85 percent river gravel and 15 percent binder soil, met all requirements for the A. A. S. H. O., type C, surface-course material specifications. Its behavior in the first phase of the track tests can be classed as fair. Some difficulty was experienced in getting this material to set up initially but thereafter, it remained stable although there was a tendency for the surface to loosen under prolonged testing with low water elevation (see fig. 3-C). Section 6 had the same composition as section 4 except for the addition of 10 percent of hydrated lime. The behavior of section 6 was excellent throughout the first phase of the testing (see table 3 and fig. 3-D).

Section 1 consisted of 90 percent limestone screenings and 10 percent binder soil. This mixture conformed to all requirements of the A. A. S. H. O. specification for type C, crusher-run surfacing materials. Its behavior like that of section 4 can be rated as fair. It was loose during the compaction period but finally set up and was stable under the applied loads. It tended to wear and become loose on top under continued traffic with low water elevation as shown in figure 3-A.

Section 3 consisted of 80 percent slag screenings and 20 percent binder soil. This mixture had a plasticity index of 7, the highest of any tested in this investigation. During the compaction period and while testing with water 1 inch above the top of the subbase, this section was unstable and exhibited considerable movement under traffic. When the water level was lowered, the stability of the section improved but wear on the surface was considerable.

(Continued on p. 190)

# POSSIBLE SUBSTITUTES FOR ALUMINUM PAINT

By E. F. HICKSON, Chemist, National Bureau of Standards, and H. A. GARDNER, Chemical Engineer, The Institute of Paint and Varnish Research

*Editor's note:* As a result of the present need to conserve aluminum, the Office of Production Management has been giving attention to the uses of aluminum paint, including those in which the substitution of some other paint is entirely feasible and those in which a satisfactory substitution is difficult.

The Office of Production Management is endeavoring to allot a limited amount of aluminum powder and paste for those few uses where aluminum paint is deemed essential and where substitution is difficult. Therefore, each order for aluminum powder and paste for paint that is placed with the producing companies is reviewed on the basis of technical considerations regarding its use, and the material is released only for the most urgent defense purposes. Other protective and decorative coatings must be substituted in the majority of instances where aluminum paint has been employed in the past.

The Office of Production Management has requested the Public Roads Administration to bring this information to the attention of the administrative officials of the State highway departments.

As is the case with many other materials which are critical during the present National Emergency, such as tung oil, shellac, etc., we know of no one paint that has all the desirable properties of aluminum paint for special uses. We have in mind such properties as durability, visibility, low emissivity, impermeability to moisture, reflectivity, opacity, etc. For example, for certain specialized purposes, such as for aircraft use, where light weight, good reflectivity and good durability in sea water are necessary, as a heat-resisting paint (above 600° F.), as a coating for low-temperature (cold storage) and refrigeration plants, as an anti-bleeding, weather-resisting and light-colored coating for bituminous roofing, etc., it is difficult at the moment to suggest a universally satisfactory alternate for aluminum paint. There are, however, a number of types of paint which are available, and which if used for the particular purpose indicated, should prove satisfactory. It is with this in mind that the following recommendations are made:

*Painting structural steel (bridges, tanks, etc.).*—After priming the clean surface with a rust-resisting primer, such as red lead paint (F. S. TT-P-86),<sup>1</sup> basic lead chromate paint (F. S. TT-P-59) etc., use a finish coat (instead of aluminum) of gray paint (or any other tint) conforming to Federal Specification TT-P-36a or TT-P-156. If chalk-resistant titanium oxide is specified, Federal Specification TT-P-101a or War Department Cantonment Paint, Standard Specification 8000E, page 88, June 30, 1941, may also be used, tinted gray or any other desired color. If color is of no moment, dark-colored paints such as iron oxide (F. S. TT-P-31a) or black (F. S. TT-P-61) will be more durable than white or light-tint paints. The black and iron oxide paints will be just about as durable as aluminum paint. Additional information on painting structural steel may be found in National Bureau of Standards Letter Circular 422.

If light or heat reflectivity is the important factor, such as in the case of gasoline-storage tanks, then a white paint on a titanium-lead-zinc base (F. S. TT-P-101a) may be used. This is a durable paint, but not as durable as aluminum paint, but is said to be more

efficient in preventing gas losses. Special proprietary "Tank White" paints have also been developed for this purpose.

*Painting interiors; plaster walls and woodwork.*—Use one coat of a primer and sealer, such as is covered by Federal Specification TT-P-56, followed by a coat of either eggshell flat wall paint (F. S. TT-P-51a) or gloss enamel (F. S. TT-E-506a).

*Priming exterior wood.*—For this purpose, for which aluminum paint has been used to some extent, use either Federal Specification TT-P-36a, TT-P-101a, TT-P-156, or one of the proprietary special undercoaters. One pint of linseed oil should be added to each gallon of the Federal Specification paints.

*Sealing knots.*—A thin coat of shellac varnish, a heavy coat of white lead paint, or one of the brands of special prepared paint undercoaters may be used.

*Prevention of bleeding of bituminous coatings.*—A good resin emulsion paint (F. S. TT-P-88) is suggested for interior use and has, in fact, been used successfully outdoors on Robertson (bituminous) protected metal. It prevents bleeding and serves as a primer.

*Painting metal roofs.*—On tin and other metal roofs where aluminum paint has been used increasingly of late, a good red metallic iron oxide roof paint (F. S. TT-P-31a) should be used. Red lead paint (F. S. TT-P-86) makes an excellent primer. Prepared metal paints made on a rust inhibitive pigment base well serve the purpose.

*Painting smokestacks, boiler fronts, etc.*—A good grade of black asphalt varnish (TT-V-51), a heat-resisting gray or black enamel, or certain of the proprietary heat-resisting compositions may be used.

*Painting interior structural steel.*—In industrial plants where good light reflection from the structural steel is desired, the following procedure may be used. Apply a priming coat of quick-drying red lead paint (Procurement Division Specification No. 358), followed by either two coats of eggshell flat white paint (F. S. TT-P-51a) or gloss white enamel, sometimes called "mill gloss white" (F. S. TT-E-506a). The enamel will be more water-resistant and more durable. For special conditions where fumes are encountered, such as in chemical laboratories, bakeries, tobacco factories, cafeterias, etc., a special enamel known as fume- and heat-resistant enamel (National Bureau of Standards Letter Circular 489) may be used.

*Machinery and metal equipment.*—A good machinery gray enamel (F. S. TT-E-506a) may be substituted in many instances.

*Radiators and hot water piping.*—The same paint used on the sidewalls may be used for this purpose. This may be eggshell flat wall paint (F. S. TT-P-51a) or white enamel (F. S. TT-E-506a). Where eggshell flat wall paint is used, we suggest the addition of one pint of interior varnish (F. S. TT-V-71a) to each gallon of the paint.

*General considerations.*—As can be seen from the foregoing, it is possible to use Federal Specification materials or their equivalents as substitutes for aluminum

<sup>1</sup>A table giving the complete designation of the Federal Specifications referred to herein will be found at the end of this article (p. 190).

paint under a variety of conditions. We have purposely avoided specifically recommending synthetic resin paints and enamels, because of the shortage of certain ingredients used in these paints. Similarly, certain highly durable cellulose finishes could be employed, but the plasticizers and solvents for these are also developing an acute shortage.

*Talc and mica-aluminum finishes.*—In cases where it is believed essential to use some aluminum powder in order to produce an aluminum appearing finish, a great saving could be effected by employing mica or talc with the aluminum powder. As high as three parts by weight of mica or talc and one part by weight of aluminum powder may be stirred into a mixing varnish to produce a finish that has the characteristic aluminum appearance. This is in the proportion of two pounds of the total pigment (including the talc and aluminum powder) to one gallon of the mixing varnish. If the fine lining grade of aluminum powder (F. S. TT-A-476, Type B) is used, as little as  $\frac{1}{2}$  pound of it and  $\frac{1}{2}$  pound of mica, suitable for paint, may be mixed with 1 gallon of varnish (F. S. TT-V-81a) to produce a paint which is reported to have good durability.

Wherever Federal Specifications are referred to in this memorandum, they cover products which will be satisfactory for the usage referred to, but for the general buying public similar products may be obtained under trade brands at any paint store throughout the

country. The paint dealer will readily recognize the material referred to.

Complete titles of Federal Specifications referred to in the body of the article:

<i>Federal Specification No.—</i>	<i>Title</i>
TT-P-86	Paint, Red Lead Base; Linseed-oil, Ready-Mixed.
TT-P-36a	Paints, Lead-Zinc Base, Ready-Mixed, and Semipaste, White and Tinted.
TT-P-156	Paint, White Lead Base; Basic Carbonate, Ready-Mixed, Light Tints and White.
TT-P-101a	Paint; Titanium-Zinc and Titanium-Zinc-Lead, Outside, Ready-Mixed, White.
TT-P-31a	Paints; Iron Hydroxide and Iron Oxide, Ready-Mixed and Semipaste.
TT-P-61	Paint; Ready-Mixed, and Semipaste, Black.
TT-P-56	Paint; (For) Priming Plaster Surfaces (Plaster Primer and Sealer).
TT-P-51a	Paints; Oil, Interior, Eggshell-Flat-Finish, Ready-Mixed and Semipaste, Light Tints and White.
TT-E-506a	Enamel; Interior, Gloss, Light Tints and White.
TT-V-51	Varnish, Asphalt.
TT-P-88	Paint, Paste, Resin Emulsion, Interior, Light Tints and White.
TT-V-71a	Varnish; Interior.
TT-V-81a	Varnish; Aluminum Mixing.
TT-P-59	Paint, International Orange.
TT-A-476	Aluminum-Powder (For) Paints (Aluminum-Bronze-Powder).

(Continued from p. 188)

*Performance with surface application of lignin binder.*—Sections 5 and 6, which contained hydrated lime and had given good service when tested as surface courses in the first phase of the investigation, became unstable when subjected to traffic after the application of lignin binder on the surface. They were so soft and shovelled so badly that it was necessary to scarify them at 205,150 wheel-trips. After the mixtures had dried out and were recompacted, they gradually set up under traffic and by the end of the second phase of testing they were in satisfactory condition to receive a bituminous surface treatment.

Section 3, slag and binder soil, was also unstable during the compaction period after the application of the lignin binder. However, it was not necessary to scarify this section and its behavior gradually improved under continued traffic. Some raveling of the surface was noted toward the end of the second phase of the testing.

Section 2, granite and binder soil, was stable during the compaction period but when water was raised to 1 inch above the top of the subbase it showed a tendency to shove under traffic for a time. The condition gradually improved under continued traffic as shown in table 3. The behavior of section 4, gravel and soil binder, was similar to that of section 2.

Section 1, limestone and binder soil, remained in good condition throughout the entire period of testing after the application of the lignin binder except for slight raveling near the end of the second phase of the testing.

In general, the application of the diluted lignin binder tended to cause softening and instability under traffic for a time. This condition gradually improved as traffic was continued. Thereafter, the sections remained stable and while the lignin binder did not prevent raveling, it appeared to retard it somewhat as compared with the tests on untreated sections.

*Performance as base courses.*—All six sections gave good performance when tested as base courses for a thin bituminous surface treatment with water  $\frac{1}{2}$  inch above the top of the subbase. Previous investigations had shown that concentrated traffic with this ground water condition provides a condition sufficiently severe to identify the definitely unsatisfactory materials.

With the water elevation raised to  $2\frac{1}{2}$  inches above the top of the sub-base, section 5 (granite, soil, and hydrated lime) began to move under traffic and had failed completely at the end of the tests with the water  $4\frac{1}{2}$  inches above the top of the subbase (see fig. 5-E). Section 2, granite and soil, was also exhibiting considerable movement under the wheels at the end of the test although the displacements as measured by the profilometers were not excessive. The remaining four sections were in good condition throughout the third phase of the track investigations.

#### CONCLUSIONS

The following conclusions appear to be justified for the sections considered as surface courses without lignin binder treatment:

1. Mixtures of limestone screenings and soil (section 1), slag screenings and soil (sec. 3) and gravel and soil (sec. 4) meeting the requirements of the A. A. S. H. O. specifications for type C surface-course materials gave fair to good service when tested with distributed traffic.

2. The combination of granite screenings and binder soil (sec. 2) which met the grading but not the plasticity index requirements of the same specifications gave poor service.

3. The addition of 10 percent of hydrated lime improved the performance of both the granite-soil and the gravel-soil mixtures (secs. 5 and 6).

For the sections considered as surface courses after

treatment with lignin binder, the tests showed that:

4. The performance of section 2 was materially improved. Raveling was prevented for the duration of the tests in section 4 and was delayed to some extent in sections 1 and 3. Both sections 5 and 6, which contained hydrated lime, became soft and unstable but after scarifying and reworking the condition of these sections improved under traffic.

For the sections considered as base courses, it was found that:

5. All of the mixtures gave satisfactory service under normal conditions of moisture. Under extreme con-

ditions, with the water elevation at 4½ inches above the top of the subbase, the two sections containing the granite screenings became unstable, section 5 which had the hydrated lime admixture failing completely. Previous investigations have indicated that this behavior could have been anticipated from the laboratory tests performed on the materials prior to the addition of lignin binder.

It is therefore concluded that the use of lignin binder in base courses under thin bituminous surface treatments does not affect the performance of base-course materials, either adversely or beneficially.

(Continued from p. 182)



FIGURE 23.—THREE STEPS IN MAKING A DENSITY TEST: A, REMOVING LOOSENED BASE COURSE MATERIAL FROM HOLE; B, WEIGHING THE BASE COURSE MATERIAL REMOVED; AND C, FILLING HOLE WITH OIL.



FIGURE 24.—BY DETERMINING THE WEIGHT OF OIL REMAINING IN THE CAN, THE WEIGHT AND VOLUME OF OIL REQUIRED TO FILL THE HOLE ARE DETERMINED.

After the moisture content of the material removed from the hole was determined, the dry density of the base in pounds per cubic foot was computed by the formula:

$$\text{Dry density} = \frac{\text{wet density} \times 100}{\text{percentage of moisture} + 100}$$

For a rapid calculation of the density in the field, the chart shown on figure 25 was used. In one of the tests, the weight of oil in the hole was 5.2 pounds, and the weight of moist material removed from the hole was 12.65 pounds. The weight of the oil is spotted on the chart at point A. This corresponds to a volume of 0.0929 cubic foot at point B.

A vertical line from point B intersects the curve corresponding to 12.65 pounds of moist material at point C. The wet density of 136.2 pounds per cubic

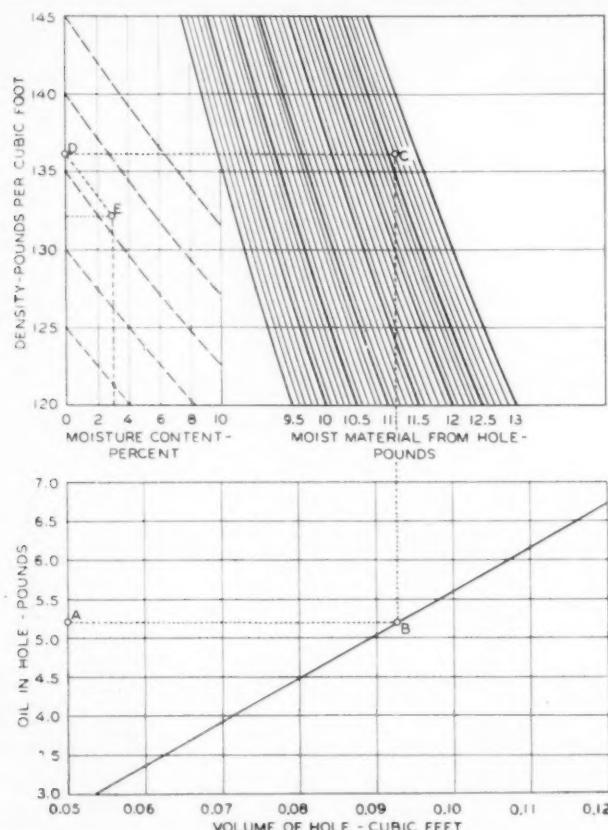


FIGURE 25.—GRAPHICAL CALCULATION OF DENSITY FROM TEST DATA

foot is indicated at point D on the density scale. With a moisture content of 3 percent the dry density of 132.2 pounds per cubic foot is found at point E. This chart was set up to cover the ranges in weights, volumes, and densities encountered on this particular project.

The sampling and testing in the portable field labora-

tory were performed by two trained operators with the aid of five laborers. The following is a list of the equipment used:

- 3 sets of sieves, each set consisting of pan and cover and sieves with square openings as follows: 3-inch, 2-inch, 1½-inch, 1-inch, ¾-inch, ⅜-inch, No. 4, No. 10, No. 40, No. 200.
  - 4 No. 10 sieves.
  - 4 No. 200 sieves.
  - 3 No. 40 sieves.
  - 1 metric solution balance, 5 kilograms capacity.
  - 1 triple beam balance, 100 grams capacity.
  - 4 double-burner gasoline camp stoves.
  - 1 enameled pan, 10 inches diameter by 4 inches deep.
  - 1 enameled pan, 14 inches diameter by 1½ inches deep.
  - 6 enameled pans, 8 inches diameter by 1½ inches deep.
  - 1 enameled pan, 6 inches diameter by 1½ inches deep.
  - 24 tin pans, 11½ inches long, 8½ inches wide, 1½ inches deep.
  - 1 pan brush, 2-inch diameter.
  - 1 pan brush, 1-inch diameter.
  - 2 brass wire brushes for sieves.
  - 3 rubber-covered pestles.
  - 2 iron pots, 10-inch diameter by 4 inches deep.
  - 1 spoon, 12 inches long.
  - 4 spoons, 14 inches long.
  - 1 mason's trowel, 7 inches long.
  - 1 Fahrenheit thermometer.
  - 4 porcelain evaporating dishes, 3-inch diameter.
  - 1 gasoline storage can, 5 gallons.
  - 1 water storage tank, 30 gallons.
  - 1 long handle shovel.
  - 1 short handle shovel.
  - 1 pick.
  - 2 soil collecting trays for density tests.
  - 1 spring scale, 30 pounds capacity.
  - 1 oil can with spout, 3 gallons capacity.
  - 1 tin pail, 2 gallons capacity.
  - 1 grease suction pump.
  - 1 garden trowel.
  - 1 pointed bar, 1½-inch diameter, 30 inches long.
  - 3 clip boards.
  - 1 slide rule.
  - 1 triangle.
  - 1 water cooler and paper cups.
- Supply of canvas sample bags, tags, twine, pencils, notebooks, cross section paper, waste rags, towels, and laboratory forms.

In addition to the above, the laboratory was supplied with work tables, shelves, chairs, fire extinguishers, an office desk, and miscellaneous office supplies.

#### INDEX TO PUBLIC ROADS, VOLUME 21, NOW AVAILABLE

The index to PUBLIC ROADS, volume 21, is now available. A chronological list of articles and a list of authors are included with the index. The index will be sent free to subscribers to PUBLIC ROADS requesting it. Requests should be addressed to the Public Administration, Roads Federal Works Agency, Washington, D. C.

Indexes to volumes 6 to 8 and 10 to 20, inclusive, are also available and will be sent to PUBLIC ROADS subscribers upon request. Indexes to volumes 1 to 5, inclusive, have never been prepared. The supply of the index to volume 9 is exhausted.



**DISPOSITION OF STATE MOTOR - VEHICLE RECEIPTS - 1940**

JOURNAL OF CLIMATE AND METEOROLOGY

## DISPOSITION OF STATE MOTOR-CARRIER TAX RECEIPTS - 1940

COMPILED FOR CALENDAR YEAR FROM REPORTS OF STATE AUTHORITIES

STATE	NET RECEIPTS OF CALENDAR YEAR	ADJUSTMENTS DUE TO UNDISTRIBUTED FUNDING UNITS	EXPENSES OF COLLECTION AND DISTRIBUTION	FOR STATE HIGHWAY PURPOSES				FOR LOCAL ROADS AND STREETS				FOR NON-HIGHWAY PURPOSES			
				CONSTRUCTION, MAINTENANCE, AND ADMINISTRATION		SERVICE OF STATE HIGHWAY OBIGATIONS		TOTAL FOR STATE HIGHWAY PURPOSES		FOR WORK ON COUNTY FOREST ROADS		TO STATE GENERAL FUNDS		FOR STATE PARKS	
				STATE HIGHWAY POLICE	STATE HIGHWAY PARK AND FOREST ROADS	STATE HIGHWAY BONDS	STATE HIGHWAY BONDS	STATE HIGHWAY BONDS	STATE HIGHWAY BONDS	CITY STREETS	LOCAL ROADS	CITY STREETS	LOCAL ROADS	CITY STREETS	LOCAL ROADS
DOLLARS	DOLLARS	DOLLARS	DOLLARS	DOLLARS	DOLLARS	DOLLARS	DOLLARS	DOLLARS	DOLLARS	DOLLARS	DOLLARS	DOLLARS	DOLLARS	DOLLARS	DOLLARS
ALABAMA	348	19	1,000	1,000	1,000	1,000	1,000	1,000	1,000	1,000	1,000	1,000	1,000	1,000	1,000
ARIZONA	185	16	201	39	59	281	1	6	282	9	1	9	-	-	-
CALIFORNIA	3,155	3	2,611	3	155	155	-	-	161	-	-	1	-	-	-
COLORADO	781	-61	2,914	463	101	1	-	-	101	4	-	4	2,346	2,346	2,346
CONNECTICUT	320	-8	723	119	119	12	73	21	21	310	73	310	-	-	-
DELAWARE	(8)	-	328	71	119	-	-	-	-	117	-	-	-	-	-
FLORIDA	361	-	261	75	-	-	-	-	-	11	270	-	5	-	5
GEORGIA	90	-9	87	68	19	-	-	-	-	19	-	-	-	-	-
IDAHO	64	7	71	20	20	-	-	-	-	51	-	-	-	-	-
ILLINOIS	1,472	-78	1,398	107	706	-	35	-	-	761	425	76	-	-	45
INDIANA	1,412	-32	1,380	99	48	-	-	-	-	37	37	-	501	45	-
KANSAS	1,417	-11	1,411	54	79	14	23	70	93	816	425	-	205	-	-
KENTUCKY	1,557	-	1,468	22	272	5	5	-	-	277	37	-	253	-	-
Louisiana	113	113	113	22	-	-	-	-	-	91	-	-	91	-	-
MARYLAND	(9)	-	19	19	-	-	-	-	-	-	-	-	-	-	-
MASSACHUSETTS	552	-	1,201	46	-	-	-	-	-	-	-	-	136	-	136
MICHIGAN	501	-	2,355	866	-	-	-	-	-	-	-	-	-	-	-
MINNESOTA	43	43	43	42	1	-	-	-	-	1	-	-	-	-	-
MISSISSIPPI	165	-	165	46	-	-	-	-	-	619	-	-	119	-	-
MISSOURI	866	-772	96	98	-	-	-	-	-	-	-	-	-	-	-
NEBRASKA	60	4	64	68	-	-	-	-	-	-	-	-	-	-	-
NEW HAMPSHIRE	37	-	260	37	-	-	-	-	-	-	-	-	-	-	-
NEW JERSEY	3	-4	260	11	216	-	33	-	-	249	-	-	-	-	-
NEW YORK	100	1	101	3	-	-	-	-	-	-	-	-	-	-	-
RHODE ISLAND	224	65	289	55	238	-	-	-	-	101	-	-	-	-	-
TEXAS	36	-	36	36	230	-	-	-	-	-	-	-	-	-	-
NORTH CAROLINA	397	-	397	15	283	-	-	-	-	382	(2)	-	-	-	-
NORTH DAKOTA	42	-	42	42	42	-	-	-	-	-	-	-	-	-	-
OHIO	598	24	622	102	387	-	-	-	-	133	-	-	-	-	-
OKLAHOMA	204	47	251	25	139	-	-	-	-	87	-	-	-	-	-
OREGON	1,357	3	1,260	213	708	49	202	1	203	960	4177	177	-	10	10
PENNSYLVANIA	5	-	5	-	5	-	-	-	-	5	-	-	-	-	-
RHODE ISLAND	9	-	9	-	9	-	-	-	-	-	-	-	-	-	-
SOUTH CAROLINA	268	-15	253	73	156	-	-	-	-	150	-	-	-	-	-
SOUTH DAKOTA	433	26	459	29	405	3	4	-	-	412	-	-	18	-	18
TEXAS	51	-	51	27	-	-	-	-	-	24	-	-	24	-	24
UTAH	123	-	122	115	8	-	-	-	-	8	-	-	-	-	-
VERMONT	(8)	-1	81	9	72	-	-	-	-	72	-	-	-	-	-
VIRGINIA	263	-1	262	54	293	9	4	-	-	306	2	2	-	-	-
WASHINGTON	174	-	174	-	-	-	-	-	-	-	-	-	-	-	-
WEST VIRGINIA	4,692	-	1,692	53	67	-	-	-	-	120	-	-	-	-	-
WISCONSIN	292	6	298	27	265	6	-	-	-	271	-	-	1,602	-	1,602
DISTRICT OF COLUMBIA	248	-	245	-	-	-	-	-	-	-	-	-	248	-	248
TOTAL	17,913	-195	17,718	3,326	6,427	4	214	470	132	662	7,637	1,760	270	4,480	5
													10	4,495	TOTAL

<sup>1/</sup> AMOUNTS DISTRIBUTED DURING THE CALENDAR YEAR DIFFER FROM ACTUAL COLLECTIONS BECAUSE OF UNDISTRIBUTED FUNDS AND LAG BETWEEN ACCOUNTS OF COLLECTING AND EXPANDING AGENCIES.

<sup>2/</sup> IN MANY STATES THE PROCEEDS OF HIGHWAY-CARRIER TAXES ARE PLACED IN A COMMON FUND FROM WHICH A DISTRIBUTION IS MADE. THE AMOUNTS SO DISTRIBUTED HAVE BEEN PRORATED IN PROPORTION TO THE RECEIPTS NOT OTHERWISE INDICATED. SEE TABLES G-2 AND M-2.

<sup>3/</sup> APPROXIMATELY \$118,000 FOR USE ON COUNTY ROADS UNDER STATE CONTROL, IN NORTH CAROLINA INCLUDED IN ALLOTMENTS FOR STATE HIGHWAY PURPOSES.

<sup>4/</sup> AMOUNTS DISTRIBUTED FOR STATE HIGHWAY PURPOSES, ON TABLE M-2 FOR 1939 AND PRIOR YEARS.

<sup>5/</sup> REIMBURSEMENT TO COUNTIES AND LOCAL UNITS OF CONTROL FOR AMOUNTS PAID BY MOTOR CARRIERS IN LIEU OF REGISTRATION FEES INCLUDED IN STATE HIGHWAY PURPOSES, ON TABLE M-2.

<sup>6/</sup> IN STATES INDICATED BY STAR (\*) THESE FUNDS MAY ALSO BE USED FOR SERVICE OF LOCAL HIGHWAY OBLIGATIONS. AMOUNTS SO USED NOT REPORTED SEPARATELY. IN COLORADO FUNDS MAY BE USED ON BOTH STATE AND LOCAL ROADS.

<sup>7/</sup> THIS COLUMN SHOWS SPECIFIC ALLOTTMENTS FOR CITY STREETS, WHERE REPORTED SEPARATELY, FUNDS ALLOCATED FOR URBAN EXTENSIONS OF STATE HIGHWAY SYSTEM ARE INCLUDED IN ALLOTMENTS FOR STATE HIGHWAY PURPOSES.

<sup>8/</sup> NO SPECIAL TAXES ON MOTOR CARRIERS REPORTED.

<sup>9/</sup> NO MILEAGE AND PASSENGER-MILE TAXES PAID BY MOTOR CARRIERS IN LIEU OF REGISTRATION FEES INCLUDED IN MOTOR-VEHICLE RECEIPTS, TABLE M-2.

<sup>10/</sup> MOTOR-CARRIER TAXES NO LONGER IMPOSED. AMOUNTS SHOWN REPRESENT DISTRIBUTION OF REVENUES COLLECTED IN PRIOR YEARS.

**DISPOSITION OF RECEIPTS FROM STATE IMPOSTS ON HIGHWAY USERS - 1940**

THE JOURNAL OF CLIMATE

## STATUS OF FEDERAL-AID HIGHWAY PROJECTS

AS OF SEPTEMBER 30, 1941

STATE	COMPLETED DURING CURRENT FISCAL YEAR			UNDER CONSTRUCTION			APPROVED FOR CONSTRUCTION		
	Estimated Total Cost	Federal Aid	Miles	Estimated Total Cost	Federal Aid	Miles	Estimated Total Cost	Federal Aid	Miles
Alabama	\$ 1,478,160	\$ 734,140	56.2	\$ 6,712,877	\$ 3,332,605	219.4	\$ 2,155,464	\$ 1,072,000	57.7
Arizona	306,896	360,976	33.1	1,520,406	1,039,990	54.7	437,998	437,998	59.2
Arkansas	1,057,900	33.0	1,189,406	523,887	45.0	641,482	320,692	38.4	
California	2,985,331	1,602,150	67.8	6,831,858	3,695,654	76.7	2,482,327	1,519,196	17.0
Colorado	1,339,304	1,016,002	102.9	2,126,406	1,234,465	113.3	946,905	531,571	65.1
Connecticut	711,755	347,250	7.2	1,782,108	872,444	22.6	1,018,029	476,221	11.9
Delaware	161,292	78,259	2.7	832,264	410,217	22.4	299,567	149,824	9.5
Florida	726,447	363,224	52.4	790,609	422,194	12.9	1,992,059	917,708	22.0
Georgia	1,734,840	861,920	60.1	6,101,204	3,165,452	260.0	1,281,611	2,140,806	116.1
Idaho	769,197	474,999	1.5	1,525,670	896,125	79.5	744,770	552,533	25.1
Illinois	2,423,110	1,205,611	54.8	8,452,162	4,226,081	151.5	1,313,272	655,654	6.8
Indiana	2,266,494	1,183,037	33.4	7,179,179	3,545,574	113.3	1,046,826	524,414	16.1
Iowa	1,687,741	794,060	79.5	5,599,070	2,946,128	126.4	1,522,001	919,200	16.3
Kansas	2,722,963	1,380,649	125.9	6,521,261	2,271,069	283.4	3,740,394	1,629,695	142.7
Kentucky	1,649,115	828,370	60.2	7,268,067	3,472,718	182.1	1,334,853	1,665,199	26.6
Louisiana	780,865	390,410	21.5	2,049,901	1,016,533	40.5	2,556,555	1,299,056	56.3
Maine	556,610	295,745	17.4	1,925,735	592,327	23.9	316,350	156,175	5.1
Maryland	1,351,200	728,000	17.6	3,616,182	1,697,678	21.0	1,145,000	242,500	5.2
Massachusetts	1,620,207	925,000	15.6	2,728,387	1,393,614	16.6	1,175,721	584,271	6.4
Michigan	4,398,630	2,195,188	80.8	5,792,910	2,885,105	124.7	1,913,900	956,950	17.8
Minnesota	2,177,891	1,384,189	252.6	10,073,327	4,998,290	451.5	1,044,893	519,562	52.2
Mississippi	1,329,000	763,140	96.9	6,820,912	3,948,466	372.1	951,270	289,100	10.3
Missouri	3,746,023	1,752,996	122.5	9,941,674	4,981,855	199.3	3,137,420	729,764	33.1
Montana	1,002,360	566,167	55.7	2,191,717	1,587,047	117.6	1,611,409	1,013,378	129.0
Nebraska	711,460	320,995	27.8	1,050,982	5,945,518	638.7	1,000,298	500,149	99.0
Nevada	1,359,580	1,162,008	60.2	2,955,679	1,092,219	60.3	507,171	340,730	9.7
New Hampshire	156,132	76,099	3.4	1,180,390	553,787	13.6	165,903	87,571	2.4
New Jersey	2,346,574	1,176,287	20.5	3,522,648	1,781,244	22.2	22,210	11,135	1,744,571
New Mexico	315,352	155,382	42.1	1,401,016	882,765	80.4	405,333	226,824	352,649
New York	3,710,494	1,859,347	60.2	11,983,517	5,958,370	136.1	609,994	304,372	1,322,902
North Carolina	2,217,874	1,071,825	98.9	3,659,747	1,932,677	106.5	910,156	589,455	36.9
North Dakota	2,216,784	1,295,546	150.4	3,126,920	1,745,672	106.5	2,255,340	1,122,040	191.4
Oklahoma	3,566,050	1,680,633	23.4	15,883,577	7,897,616	139.2	3,825,680	1,572,500	25.6
Oregon	1,150,305	673,005	51.4	2,287,291	1,734,944	96.6	1,956,370	1,030,566	58.3
Pennsylvania	1,113,009	1,445,098	37.2	4,112,297	2,204,640	80.7	2,761,948	1,207,190	20.9
Rhode Island	2,901,183	1,746,830	39.6	14,121,292	6,599,761	114.4	1,427,365	705,232	10.8
South Carolina	350,257	49.2	3.8	1,051,537	524,097	8.1	473,292	236,679	2.9
South Dakota	501,870	245,625	167.0	4,006,337	1,750,219	109.7	1,346,253	276,826	32.6
Tennessee	1,304,810	793,670	10.7	1,627,351	2,931,393	169.5	1,637,100	936,680	162.9
Texas	1,035,130	511,865	42.5	5,384,024	2,892,012	97.8	647,487	407,7	1,794,818
Utah	4,250,531	2,102,444	211.0	12,799,558	6,294,074	524.0	4,504,510	1,911,145	1,160,286
Vermont	452,206	338,102	34.5	2,345,984	1,744,008	50.6	103,599	70,212	6.0
Virginia	316,144	156,599	10.7	1,615,165	819,292	37.6	56,299	28,190	2.9
Washington	1,069,577	536,338	25.2	4,710,662	2,197,510	80.8	1,588,672	791,286	26.2
West Virginia	808,625	447,683	27.7	2,904,391	1,551,704	62.4	439,785	874,434	6.8
Wisconsin	704,085	349,450	42.5	6,357,668	3,000,686	191.7	61,970	60,955	1.0
Wyoming	52,467	360,262	16.3	1,949,404	1,220,635	150.9	1,927,172	627,400	2,277,770
District of Columbia	463,514	231,940	2.5	-463,270	231,300	2.0	310,618	124,600	17.3
Hawaii	No. 808	70,395	2.1	701,537	515,187	9.5	21,166	21,166	1.7
Puerto Rico	22,491	60,446	23.3	1,471,524	521,185	12.5	461,580	461,580	1,022,734
TOTALS	76,262,691	39,511,138	2,929.7	233,441,687	118,231,399	6,671.3	68,449,755	31,921,144	2,053.3

\$5,449,958

## **STATUSES OF FEDERAL-AID SECONDARY OR FEEDER ROAD PROJECTS**

AS OF SEPTEMBER 30, 1941

# PUBLICATIONS of the PUBLIC ROADS ADMINISTRATION

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Any of the following publications may be purchased from the Superintendent of Documents, Government Printing Office, Washington, D. C. As his office is not connected with the Agency and as the Agency does not sell publications, please send no remittance to the Federal Works Agency.

## ANNUAL REPORTS

- Report of the Chief of the Bureau of Public Roads, 1931. 10 cents.  
Report of the Chief of the Bureau of Public Roads, 1932. 5 cents.  
Report of the Chief of the Bureau of Public Roads, 1933. 5 cents.  
Report of the Chief of the Bureau of Public Roads, 1934. 10 cents.  
Report of the Chief of the Bureau of Public Roads, 1935. 5 cents.  
Report of the Chief of the Bureau of Public Roads, 1936. 10 cents.  
Report of the Chief of the Bureau of Public Roads, 1937. 10 cents.  
Report of the Chief of the Bureau of Public Roads, 1938. 10 cents.  
Report of the Chief of the Bureau of Public Roads, 1939. 10 cents.  
Work of the Public Roads Administration, 1940.

## HOUSE DOCUMENT NO. 462

- Part 1 . . . Nonuniformity of State Motor-Vehicle Traffic Laws. 15 cents.  
Part 2 . . . Skilled Investigation at the Scene of the Accident Needed to Develop Causes. 10 cents.  
Part 3 . . . Inadequacy of State Motor-Vehicle Accident Reporting. 10 cents.  
Part 4 . . . Official Inspection of Vehicles. 10 cents.  
Part 5 . . . Case Histories of Fatal Highway Accidents. 10 cents.  
Part 6 . . . The Accident-Prone Driver. 10 cents.

## MISCELLANEOUS PUBLICATIONS

- No. 76MP . . . The Results of Physical Tests of Road-Building Rock. 25 cents.  
No. 191MP . . . Roadside Improvement. 10 cents.  
No. 272MP . . . Construction of Private Driveways. 10 cents.  
No. 279MP . . . Bibliography on Highway Lighting. 5 cents.  
Highway Accidents. 10 cents.  
The Taxation of Motor Vehicles in 1932. 35 cents.  
Guides to Traffic Safety. 10 cents.  
An Economic and Statistical Analysis of Highway-Construction Expenditures. 15 cents.  
Highway Bond Calculations. 10 cents.  
Transition Curves for Highways. 60 cents.  
Highways of History. 25 cents.  
Specifications for Construction of Roads and Bridges in National Forests and National Parks. 1 dollar.

## DEPARTMENT BULLETINS

- No. 1279D . . . Rural Highway Mileage, Income, and Expenditures, 1921 and 1922. 15 cents.  
No. 1486D . . . Highway Bridge Location. 15 cents.

## TECHNICAL BULLETINS

- No. 55T . . . Highway Bridge Surveys. 20 cents.  
No. 265T . . . Electrical Equipment on Movable Bridges. 35 cents.

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Single copies of the following publications may be obtained from the Public Roads Administration upon request. They cannot be purchased from the Superintendent of Documents.

## MISCELLANEOUS PUBLICATIONS

- No. 296MP . . . Bibliography on Highway Safety.  
House Document No. 272 . . . Toll Roads and Free Roads.  
Indexes to PUBLIC ROADS, volumes 6-8 and 10-20, inclusive.

## SEPARATE REPRINT FROM THE YEARBOOK

- No. 1036Y . . . Road Work on Farm Outlets Needs Skill and Right Equipment.

## TRANSPORTATION SURVEY REPORTS

- Report of a Survey of Transportation on the State Highway System of Ohio (1927).  
Report of a Survey of Transportation on the State Highways of Vermont (1927).  
Report of a Survey of Transportation on the State Highways of New Hampshire (1927).  
Report of a Plan of Highway Improvement in the Regional Area of Cleveland, Ohio (1928).  
Report of a Survey of Transportation on the State Highways of Pennsylvania (1928).  
Report of a Survey of Traffic on the Federal-Aid Highway Systems of Eleven Western States (1930).

## UNIFORM VEHICLE CODE

- Act I.—Uniform Motor Vehicle Administration, Registration, Certificate of Title, and Antitheft Act.  
Act II.—Uniform Motor Vehicle Operators' and Chauffeurs' License Act.  
Act III.—Uniform Motor Vehicle Civil Liability Act.  
Act IV.—Uniform Motor Vehicle Safety Responsibility Act.  
Act V.—Uniform Act Regulating Traffic on Highways.  
Model Traffic Ordinances.

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A complete list of the publications of the Public Roads Administration, classified according to subject and including the more important articles in PUBLIC ROADS, may be obtained upon request addressed to Public Roads Administration, Willard Bldg., Washington, D. C.

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**STATUS OF FEDERAL-AID GRADE CROSSING PROJECTS**

**AS OF SEPTEMBER 30, 1941**

STATE	COMPLETED DURING CURRENT FISCAL YEAR				UNDER CONSTRUCTION				APPROVED FOR CONSTRUCTION				NUMBER BALANCE OF FUNDING AVAIL- ABLE FOR FEDERAL-AID PROJECTS		
	Estimated Total Cost	Federal Aid	Number	Grade Crossing Project Completed by Increases in State Road Fund Allocation and Other Sources	Federal Aid	Estimated Total Cost	Number	Grade Crossing Project Completed by Increases in State Road Fund Allocation and Other Sources	Federal Aid	Estimated Total Cost	Number	Grade Crossing Project Completed by Increases in State Road Fund Allocation and Other Sources			
Alabama	\$ 2,839	\$ 2,839	1	\$ 424,722	\$ 422,700	6	5	2	\$ 71,235	\$ 71,235	2	6	\$ 810,911		
Arizona	46,864	46,864	1	1	571,506	186,306	6	1	121,422	101,218	1	2	119,175		
Arkansas	316,205	290,769	1	1	1,309,838	1,309,835	6	1	25,827	25,827	6	5	319,519		
California	5,685	5,646	2	61,712	59,186	60,676	6	1	20,630	20,630	7	5	1,477,100		
Colorado	166,222	165,415	2	94,135	94,135	94,135	1	1	231,374	222,740	1	1	351,963		
Delaware	20,170	20,170	4	519,457	519,457	519,457	5	1	597,074	508,721	3	1	71,349		
Florida	368,009	368,009	5	1	963,425	963,425	6	1	366,006	366,006	3	24	705,692		
Georgia	11,301	11,301	26	302,225	291,533	291,533	3	1	917,048	917,048	3	5	1,133,402		
Idaho	70,851	58,755	2	2,209,791	2,002,386	2,002,386	9	1	51	421,621	421,621	1	4	261,293	
Illinois	44,259	44,259	3	1,948,152	931,668	931,668	7	1	15	228,611	228,611	1	2	1,560,359	
Indiana	77,032	75,950	1	2	1,388,262	1,310,614	11	9	429,481	429,481	1	1	619,215		
Iowa	14,071	14,071	2	290,610	599,610	599,610	9	1	348,874	348,874	5	14	129,155		
Kansas	163,064	161,519	2	1,075,261	1,069,297	1,069,297	8	1	306,574	306,574	3	14	870,883		
Kentucky				585,415	585,415	585,415	6	1	471,536	471,536	1	1	59,942		
Louisiana	164,400	132,607	2	2	368,443	386,443	386,443	6	1,261	1,261	1	1	610,731		
Maryland				344,709	344,709	344,709	2	6	293,303	446,505	2	14	117,994		
Massachusetts	359,700	359,700	1	4	1,022,124	1,010,284	1,010,284	5	1	855,642	855,642	3	2	204,759	
Michigan	226,051	226,051	1	3	1,000,152	1,000,152	1,000,152	3	1	255,632	195,471	2	26	599,154	
Minnesota	177,900	177,900	1	1	1,127,961	1,127,961	1,127,961	3	1	252,095	252,095	1	3	453,356	
Mississippi				2,034,922	1,579,502	1,579,502	6	4	235,900	235,900	2	11	432,668		
Missouri				230,745	230,745	230,745	3	1	205,995	177,526	2	2	1,154,339		
Montana				1,116,942	1,116,942	1,116,942	22	4	6,646	6,646	2	2	470,915		
Nebraska	119,280	119,280	2	1	56,484	56,484	56,484	22	4	100,552	100,552	1	12	107,255	
Nevada	63,682	62,862	2	1	303,989	303,689	303,689	4	2	21,103	21,103	1	7	684,817	
New Hampshire	214,360	214,360	2	1	1,284,863	1,129,313	1,129,313	5	2	1,255,632	1,255,632	2	2	201,894	
New Jersey				2,975,256	2,926,252	2,926,252	5	11	318,427	311,293	4	2	592,977		
New Mexico	384,228	384,228	7	13	697,230	684,293	684,293	6	3	1,129,183	1,111,183	3	1	344,481	
New York	224,980	224,980	2	1	3,485,493	3,274,490	3,274,490	15	3	543,807	543,807	2	2	2,553,712	
North Carolina	83,460	83,460	2	1	762,212	762,212	762,212	5	3	502,456	502,456	4	1	2,051,758	
North Dakota	124,301	123,904	1	1	14	14	14	125,127	84,175	84,175	2	21	1,046,952		
Ohio	122,346	121,930	5	2	125,127	84,175	84,175	2	1	1,113,991	1,113,991	2	21	1,113,991	
Oklahoma	302,166	278,255	7	2	3,247,657	3,208,226	3,208,226	17	1	1,306,206	1,306,206	3	5	390,976	
Pennsylvania	710,467	710,467	7	208,896	208,896	208,896	1	1	311,183	311,183	7	1	1,324,754		
Rhode Island	124,756	124,756	2	6	372,732	360,332	360,332	5	3	314,746	314,746	2	2	176,063	
South Carolina	341,670	341,670	10	1	596,402	640,432	640,432	12	5	166,993	166,993	1	2	685,745	
South Dakota	92,670	83,670	1	2	1,309,479	1,309,479	1,309,479	8	1	223,120	223,120	2	2	331,953	
Tennessee	646,900	649,900	7	1	1,726,891	1,726,891	1,726,891	17	1	286,750	286,750	4	1	1,046,952	
Utah	41,268	40,526	2	12	72,149	72,149	72,149	11	1	67,714	67,714	24	232,778		
Vermont	2,205	2,193			311,685	308,108	308,108	2	4	1,021,610	1,021,610	5	5	5,465	
Virginia	32,555	32,555	1	1	771,750	771,750	771,750	4	1	106,935	87,475	2	4	566,336	
Washington	55,103	52,443			333,418	333,418	333,418	5	1	58,053	58,053	2	4	451,995	
West Virginia	6,320	6,320	2	1	811,426	805,812	805,812	9	1	93,460	93,460	1	1	832,211	
Wisconsin	46,124	46,124	11	11	899,718	869,124	869,124	11	11	210,900	208,450	4	5	1,351,829	
Wyoming	477,152	477,152	5	11	4,929	4,929	4,929	5	2	6,171	6,171	24	286,114		
District of Columbia	2,193	2,193			1,462	1,462	1,462	1	1	298,213	271,744	1	1	5,993	
Puerto Rico	192,574	192,566	2	1	619,340	619,340	619,340	9	1	214,170	213,675	1	1	179,950	
TOTALS	\$ 8,116,135	7,806,136	67	21	121	41,251,347	39,825,541	295	67	151	13,157,705	12,021,977	69	24	473